

“In mathematics you don't understand things...  
...you just get used to them.”

**- John von Neumann**

([http://en.wikipedia.org/wiki/John\\_von\\_Neumann](http://en.wikipedia.org/wiki/John_von_Neumann) )

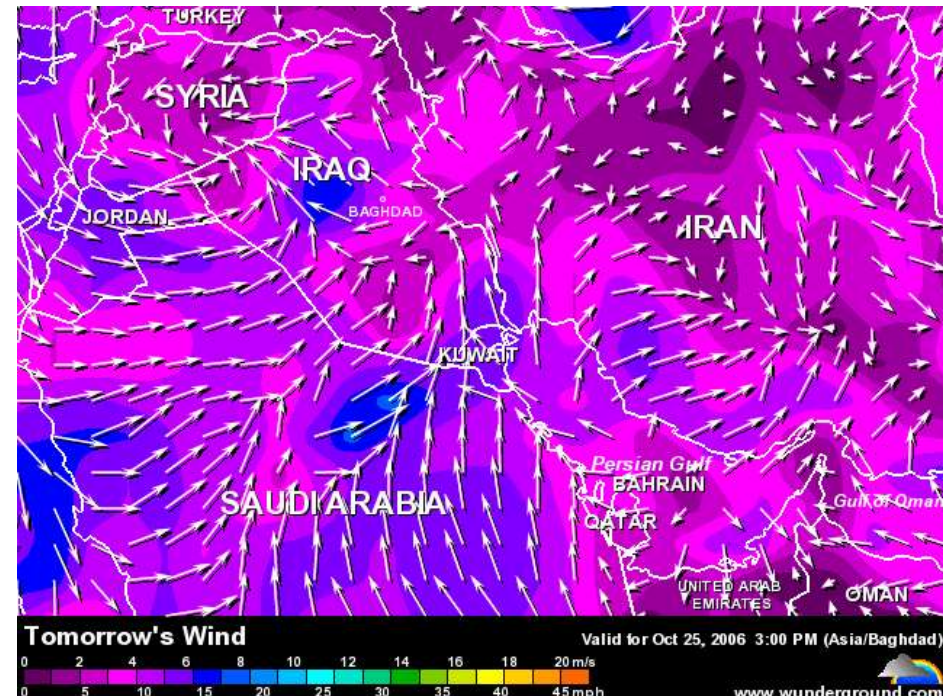
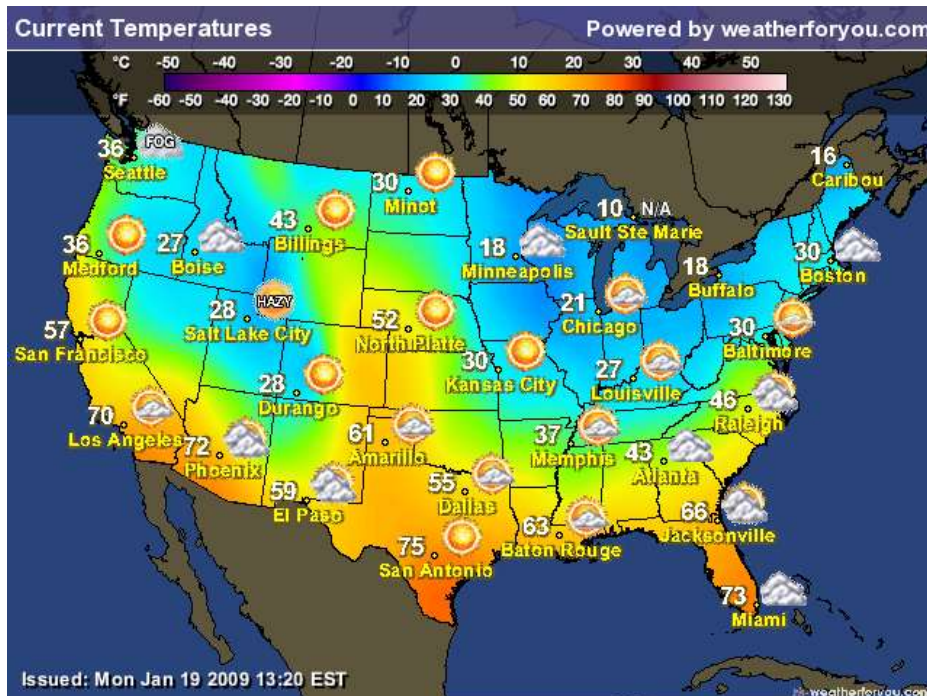
# Vector Analysis

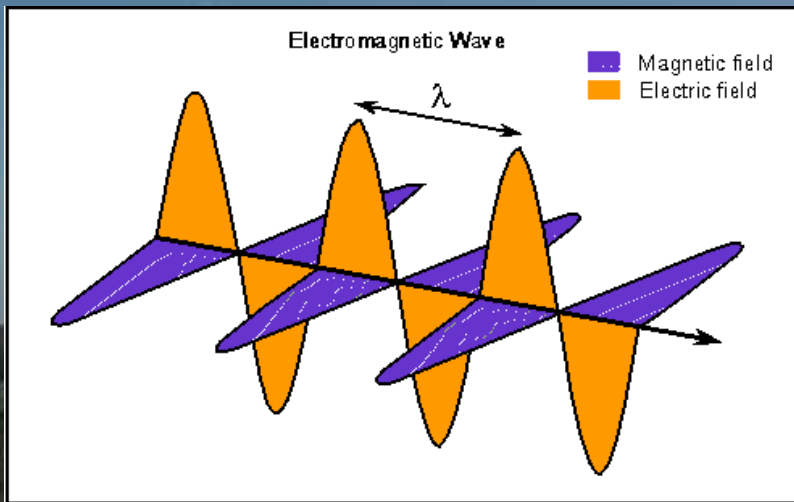
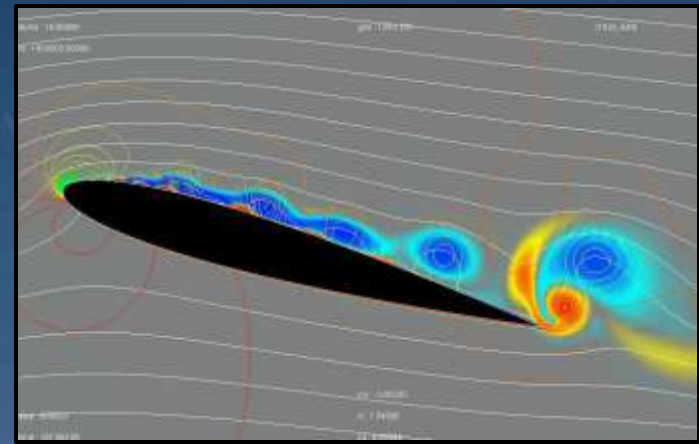
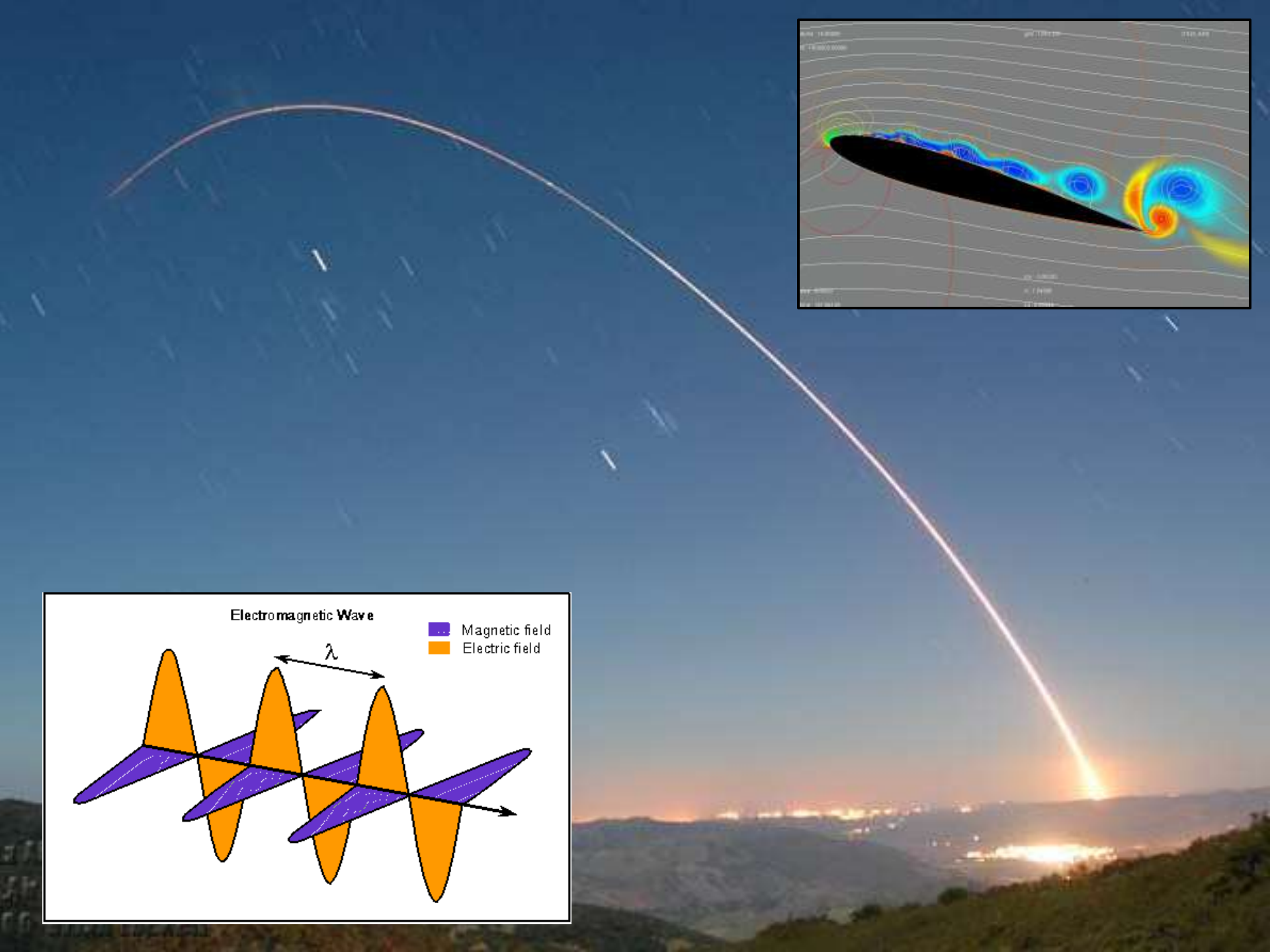
30 Jan.	Vector Analysis	3-1 thru 3-3	Lab: Analyzer This
1 Feb.	“	3-4, 3-5	
3 Feb.	“	3-6, 3-7	

*Scalar* – a quantity whose value is represented by a single real number (temperature, mass, volume)

*Vector* – a quantity whose value is represented by a magnitude and a direction in space (force, velocity, position vector)

*Field* – a function of the coordinates of every point in a region in space that defines a scalar or a vector quantity (temperature in a room, Earth's gravitational field)



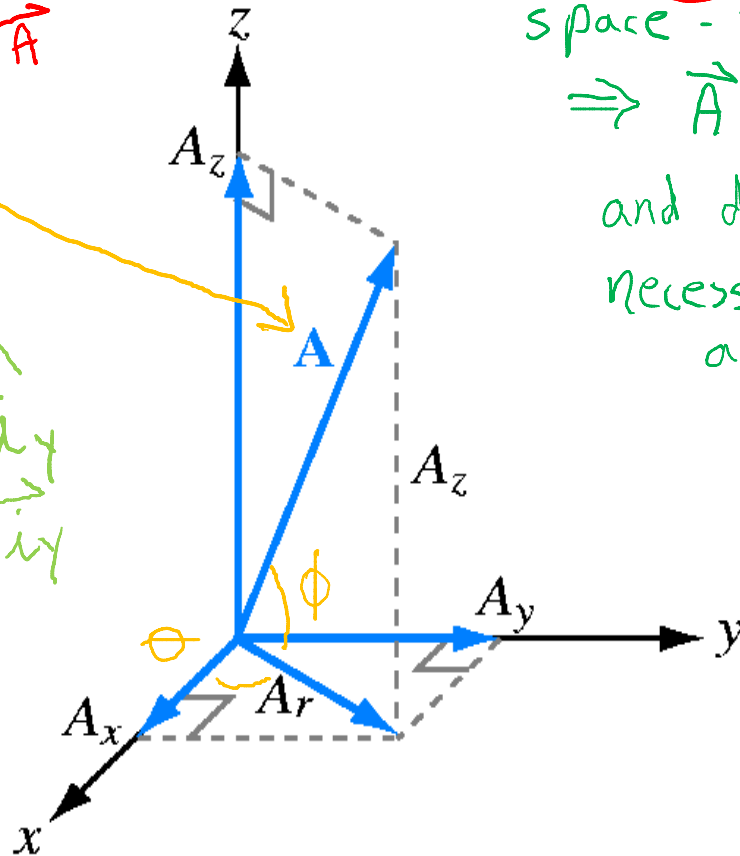
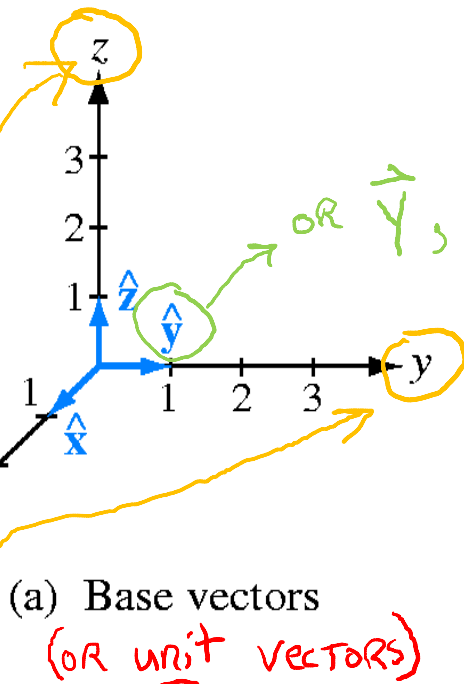


# Vectors

$$|\mathbf{A}|^2 = A_x^2 + A_y^2 + A_z^2$$

$|\mathbf{A}|$  = magnitude of  $\vec{\mathbf{A}}$

Note: a vector exists at a single point in space-time  
 $\Rightarrow \vec{\mathbf{A}}(x, y, z, t)$   
 and does not necessarily point to a location!



(b) Components of  $\mathbf{A} = \vec{\mathbf{A}}$

$$= A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$$

VECTOR

VECTOR

easier than bold when writing 😊

CARTESIAN  
 Coordinates

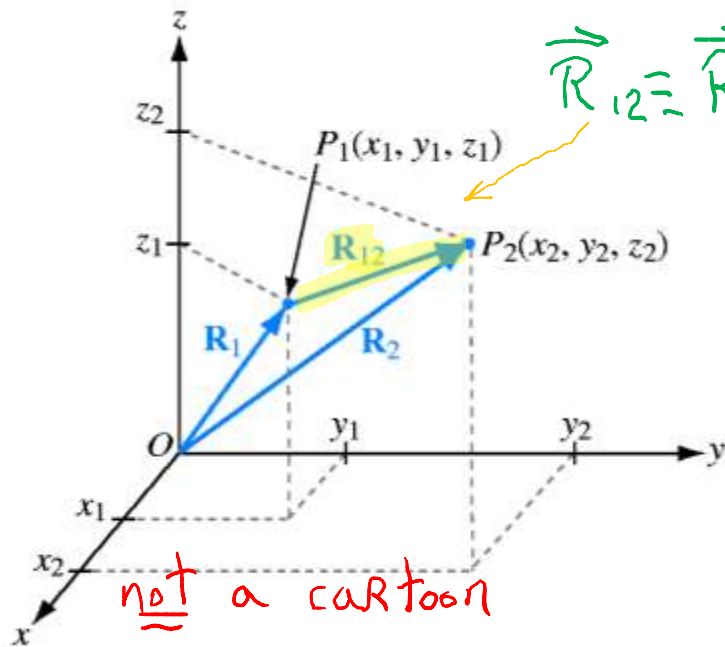


Let  $\vec{A} = A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$   
 $\vec{B} = B_x \hat{x} + B_y \hat{y} + B_z \hat{z}$  } in Cartesian  
coordinates

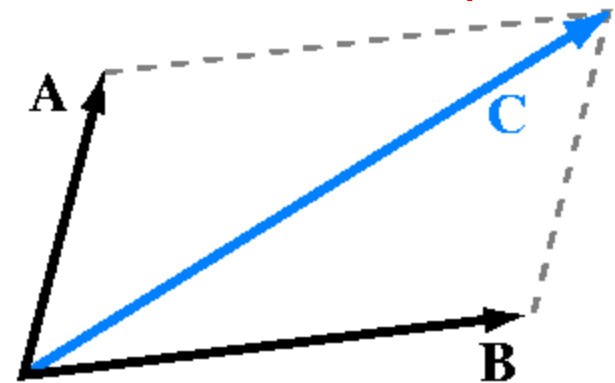
Q: What does  $\vec{A} = \vec{B}$  mean??

### Special Case

Position Vector,  $\vec{R}$ , is vector from origin to point in space, P.



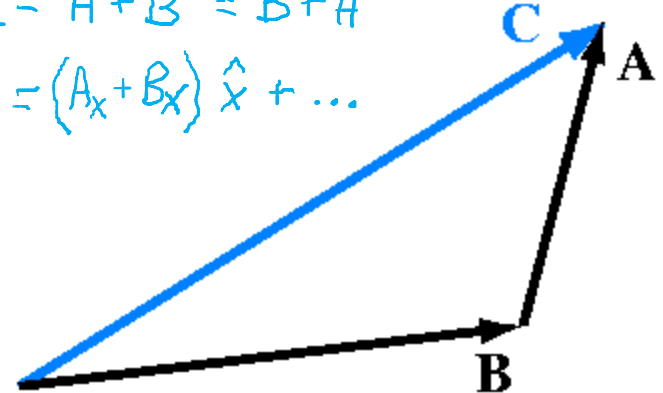
Note: this is a CARTOON



(a) Parallelogram rule

$$\vec{C} = \vec{A} + \vec{B} = \vec{B} + \vec{A}$$

$$= (A_x + B_x) \hat{x} + \dots$$



(b) Head-to-tail rule

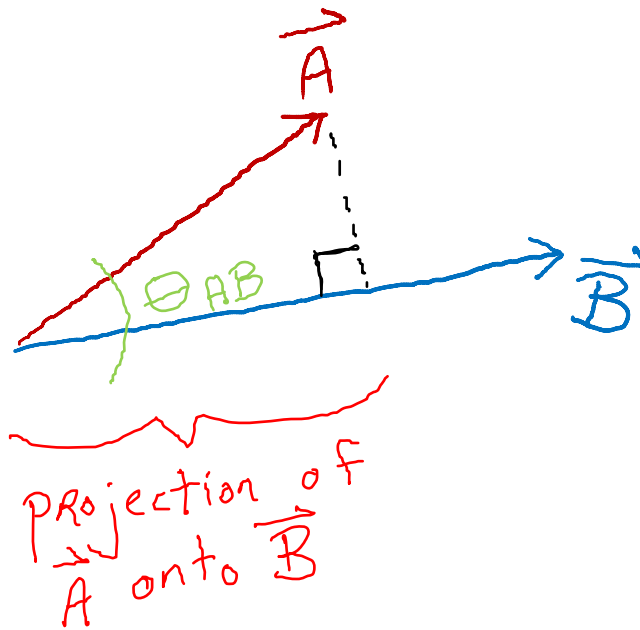
$$\vec{D} = \vec{A} - \vec{B} = \vec{A} + (-\vec{B})$$

# Dot Product

$$\vec{A} \cdot \vec{B}$$

SCALAR

$$= \vec{B} \cdot \vec{A}$$



$$|\vec{A}| |\vec{B}| \cos \theta_{AB}$$

NOTE: the dot product of any 2 normal\* vectors is zero!

\* perpendicular...

$$\vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$$

for Cartesian Coords.

$$\vec{A} \cdot \vec{A} = |\vec{A}|^2$$

Why will we care about Dot products?

Example:

Find the angle between  $\vec{A} = \hat{x}3 + \hat{y} - \hat{z}2$  and  $\vec{B} = -\hat{x} + \hat{y} + \hat{z}5$

$$|\vec{A}| = \sqrt{3^2 + 1^2 + (-2)^2} = \sqrt{14}, \quad |\vec{B}| = \sqrt{(-1)^2 + 1^2 + 5^2} = \sqrt{27}, \quad |\vec{A}||\vec{B}| \cos \phi = \sqrt{378} \cos \phi$$

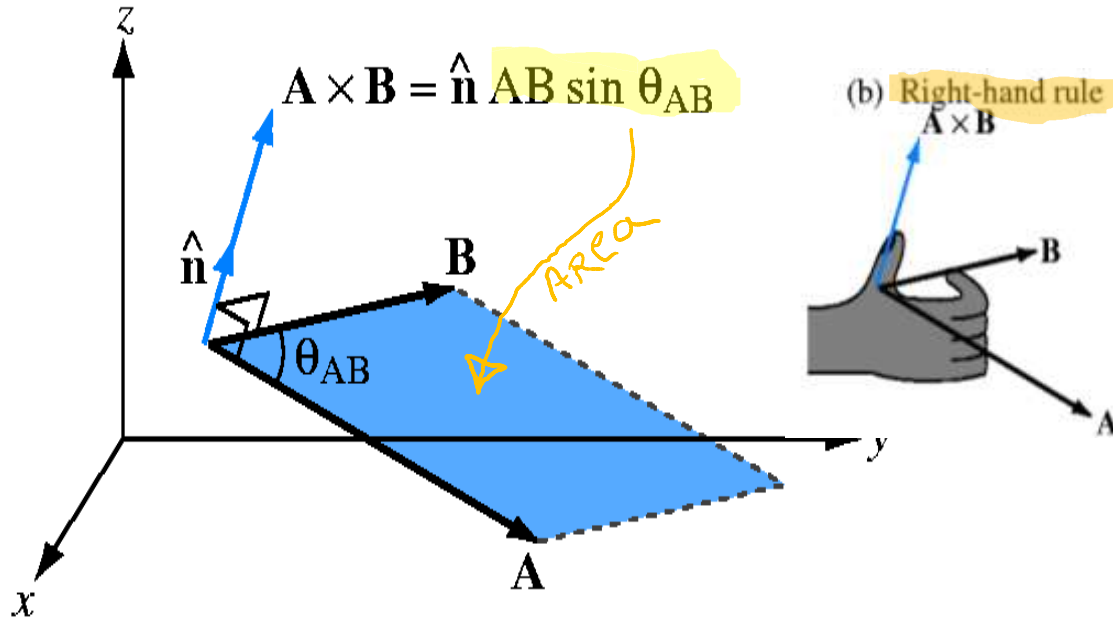
$$\vec{A} \cdot \vec{B} = 3(-1) + 1 \cdot 1 - 2 \cdot 5 = -3 + 1 - 10 = -12$$

$$\cos \phi = \frac{-12}{\sqrt{378}}, \quad \phi \approx 128^\circ$$

# Cross-Product

$$\vec{A} \times \vec{B} = \hat{n} |\vec{A}| |\vec{B}| \sin \theta_{AB} = -\vec{B} \times \vec{A}$$

a vector  $\nearrow$  normal to both  $\vec{A}$  &  $\vec{B}$



$$\vec{A} \times \vec{A} = ?$$

$$\hat{x} \times \hat{y} = ?$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

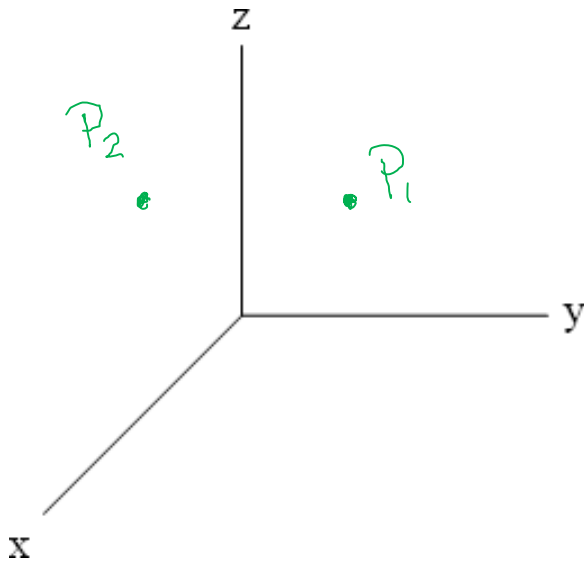
determinant

$$\Rightarrow \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix} = (A_y B_z - A_z B_y) \hat{x} + (A_z B_x - A_x B_z) \hat{y} + (A_x B_y - A_y B_x) \hat{z}$$

for Cartesian

Why will we care about cross-products?

**Exercise 3.1** Find the distance vector between  $P_1(1,2,3)$  and  $P_2(-1,-2,3)$  in Cartesian coordinates.



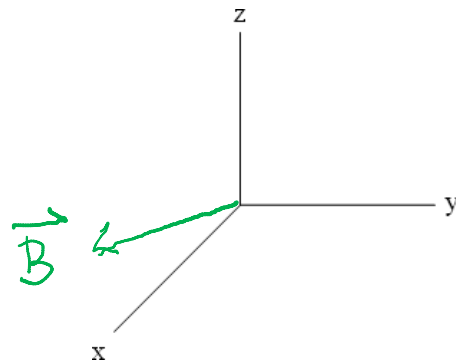
$$\begin{aligned}\vec{R}_{12} &= \vec{P_1P_2} = \hat{x}(x_2 - x_1) + \hat{y}(y_2 - y_1) + \hat{z}(z_2 - z_1) \\ &= \hat{x}(-1 - 1) + \hat{y}(-2 - 2) + \hat{z}(3 - 3) \\ &= -\hat{x}2 - \hat{y}4.\end{aligned}$$

What is the distance between  $P_1$  &  $P_2$ ?

$$\Rightarrow |\vec{R}_{12}| = \sqrt{2^2 + 4^2} \approx 4.47 \text{ units}$$

**Exercise 3.3** Find the angle that vector **B** of Example 3-1 makes with the z-axis.

$$\vec{B} = -\hat{x} - 5\hat{y} - \hat{z}$$



$$\mathbf{B} \cdot \hat{z} = B \cos \theta$$

$$(-\hat{x} - \hat{y}5 - \hat{z}) \cdot \hat{z} = \sqrt{27} \cos \theta$$

$$\cos \theta = \frac{-1}{\sqrt{27}}$$

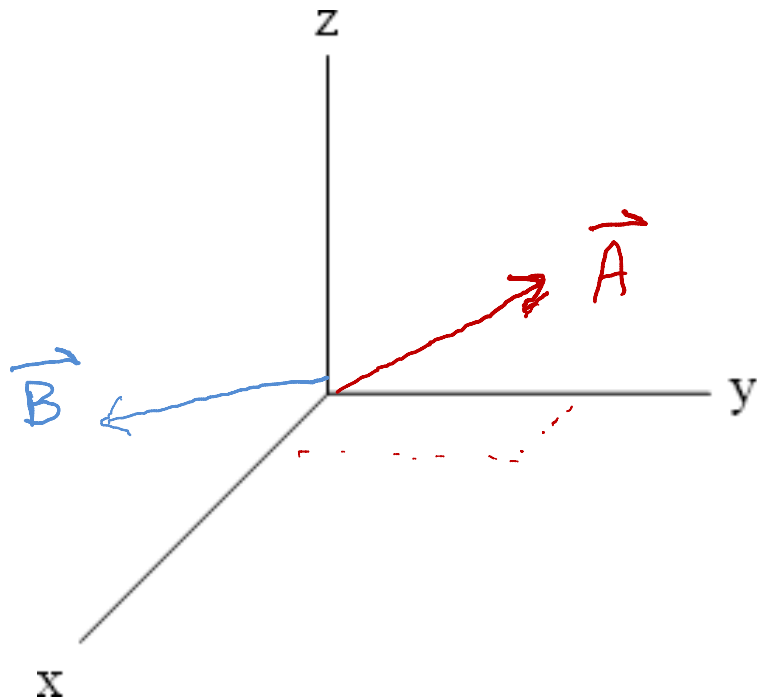
$$\theta = 101.1^\circ.$$



**Exercise 3.2** Find the angle  $\theta$  between vectors **A** and **B** of Example 3-1 using the cross product between them.

$$\vec{A} = 2\hat{x} + 3\hat{y} + 3\hat{z}$$

$$\vec{B} = -\hat{x} - 5\hat{y} - \hat{z}$$



$$\mathbf{A} \times \mathbf{B} = \hat{n}AB \sin \theta_{AB}$$

$$\begin{aligned} \sin \theta_{AB} &= \frac{|\mathbf{A} \times \mathbf{B}|}{AB} \\ &= \frac{|(\hat{x}2 + \hat{y}3 + \hat{z}3) \times (-\hat{x} - \hat{y}5 - \hat{z})|}{\sqrt{22}\sqrt{27}} \\ &= \frac{|-\hat{z}10 + \hat{y}2 + \hat{z}3 - \hat{x}3 - \hat{y}3 + \hat{x}15|}{\sqrt{22}\sqrt{27}} \\ &= \frac{|\hat{x}12 - \hat{y} - \hat{z}7|}{\sqrt{22}\sqrt{27}} = \frac{\sqrt{144 + 1 + 49}}{\sqrt{22}\sqrt{27}} = 0.57 \end{aligned}$$

$$\theta_{AB} = \sin^{-1}(0.57) = 34.9^\circ \text{ or } 145.1^\circ.$$

Q: how would you find a unit vector perpendicular to both  $\vec{A}$  and  $\vec{B}$ ?

Examples:

Find all unit vectors that are perpendicular to both

$$\vec{A} = \hat{x}3 + \hat{y} - \hat{z}2 \quad \text{and} \quad \vec{B} = -\hat{x} + \hat{y} + \hat{z}5$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 3 & 1 & -2 \\ -1 & 1 & 5 \end{vmatrix} = \hat{x}(5+2) + \hat{y}(2-15) + \hat{z}(3+1) = \hat{x}7 - \hat{y}13 + \hat{z}4$$

$$\hat{n} = \frac{\vec{A} \times \vec{B}}{|\vec{A} \times \vec{B}|} = \frac{\hat{x}7 - \hat{y}13 + \hat{z}4}{\sqrt{7^2 + (-13)^2 + 4^2}} = \frac{\hat{x}7 - \hat{y}13 + \hat{z}4}{\sqrt{234}} = \hat{x}0.46 - \hat{y}0.85 + \hat{z}0.26$$

$$-\hat{n} = -\hat{x}0.46 + \hat{y}0.85 - \hat{z}0.26 \qquad \hat{n} \perp (\vec{A}, \vec{B}) \quad \text{and} \quad -\hat{n} \perp (\vec{A}, \vec{B})$$

Which of the following products of vectors do not make sense:

a)  $(\vec{A} \cdot \vec{B}) \times \vec{C}$

c)  $\vec{A}(\vec{B} \cdot \vec{C})$

e)  $\vec{A}/\hat{a}$

b)  $(\vec{A} \times \vec{B}) \times \vec{C}$

d)  $\vec{A}/\vec{B}$

f)  $(\vec{A} \times \vec{B}) \cdot \vec{C}$

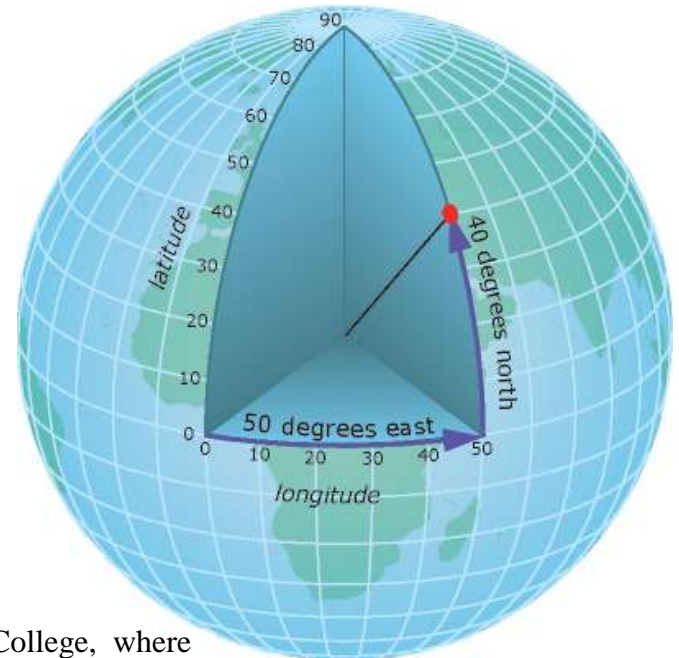
a) A scalar cannot be crossed with a vector

d) and e) Division of vectors is not defined

# Orthogonal Coordinate Systems

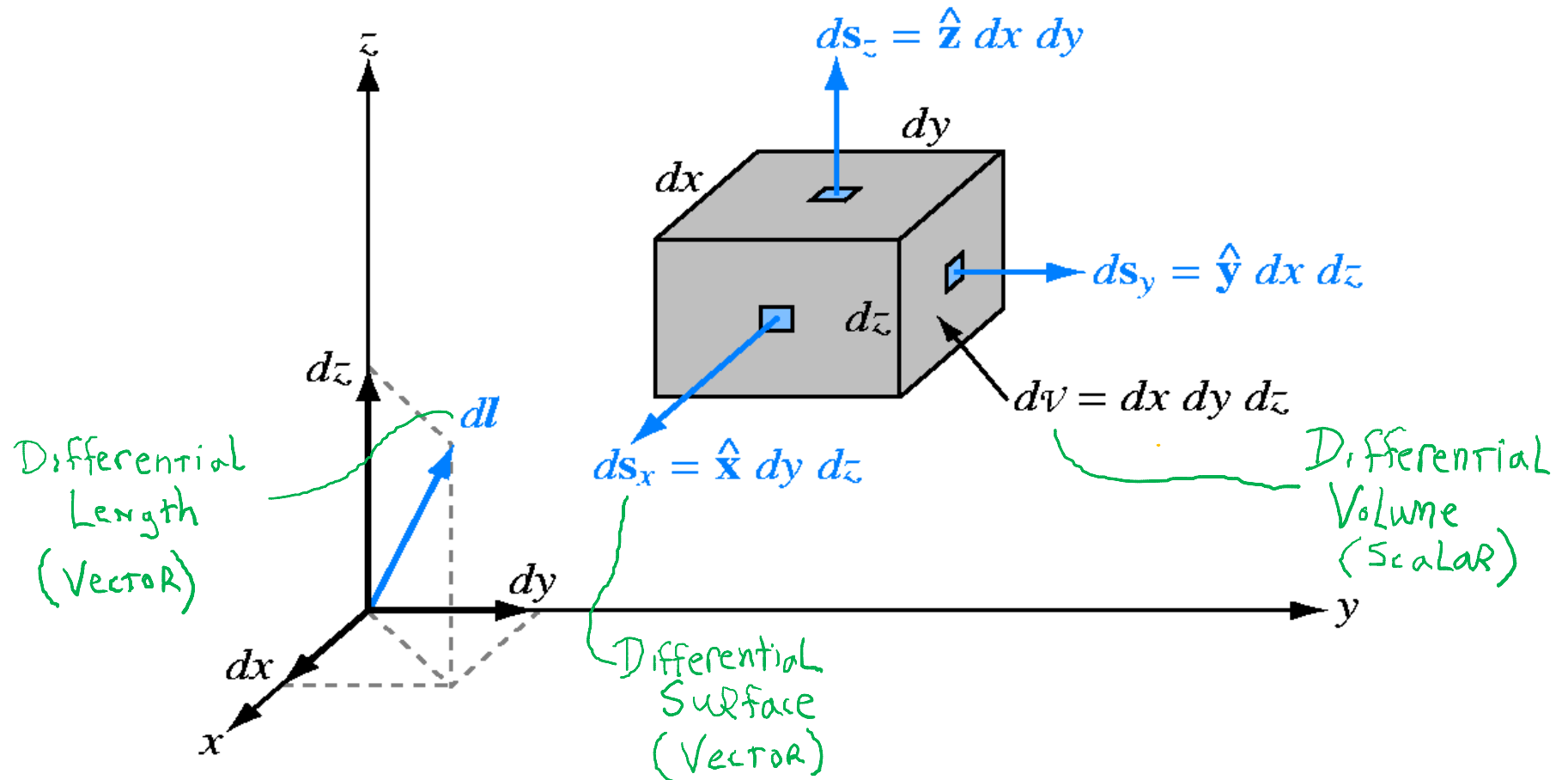
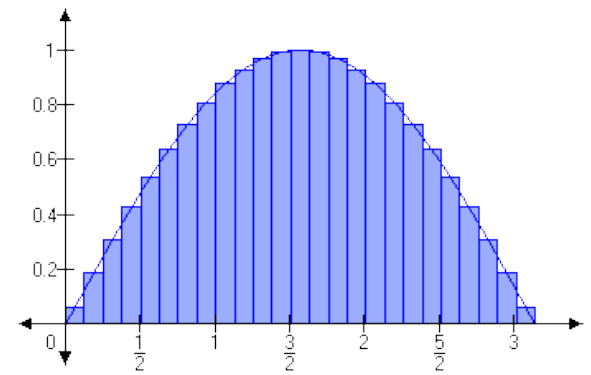


[http://en.wikipedia.org/wiki/Ren%C3%A9\\_Descartes](http://en.wikipedia.org/wiki/Ren%C3%A9_Descartes)



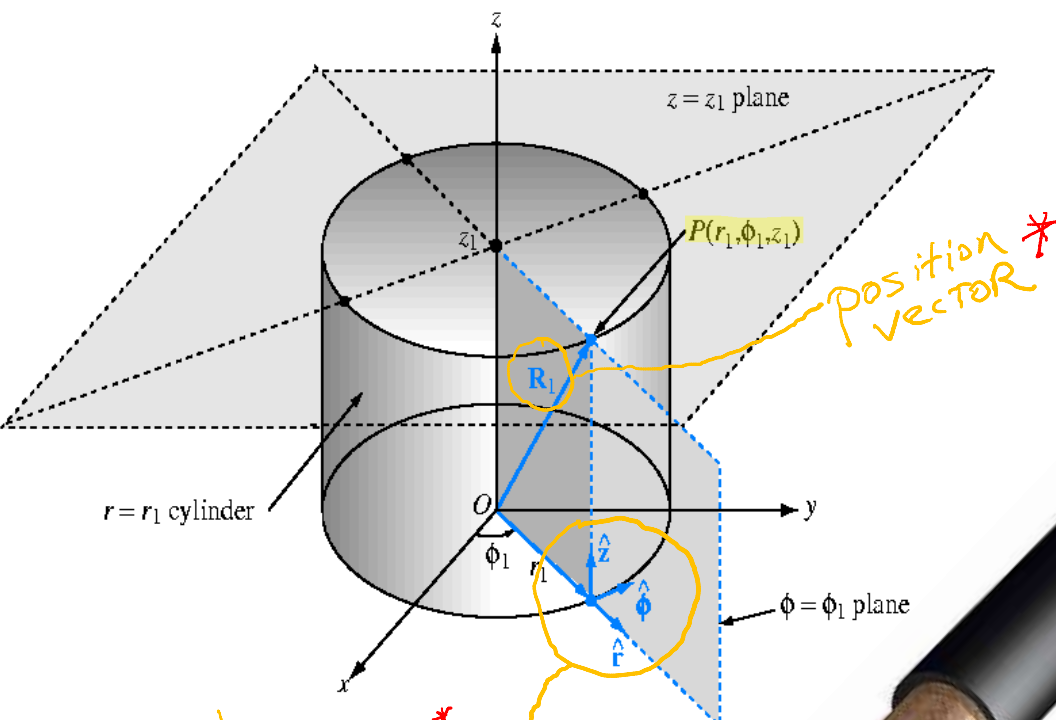
Q: if you went straight through the Earth from State College, where would you be on the other side? What would be the nearest big city?

# Calculus





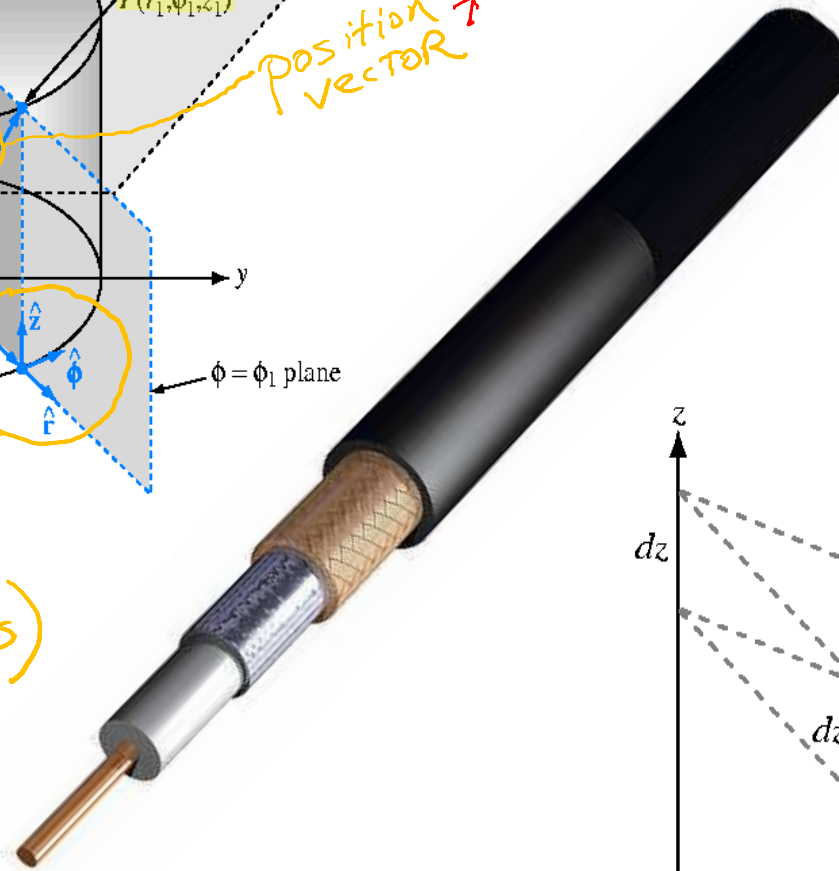
\* Note Difference



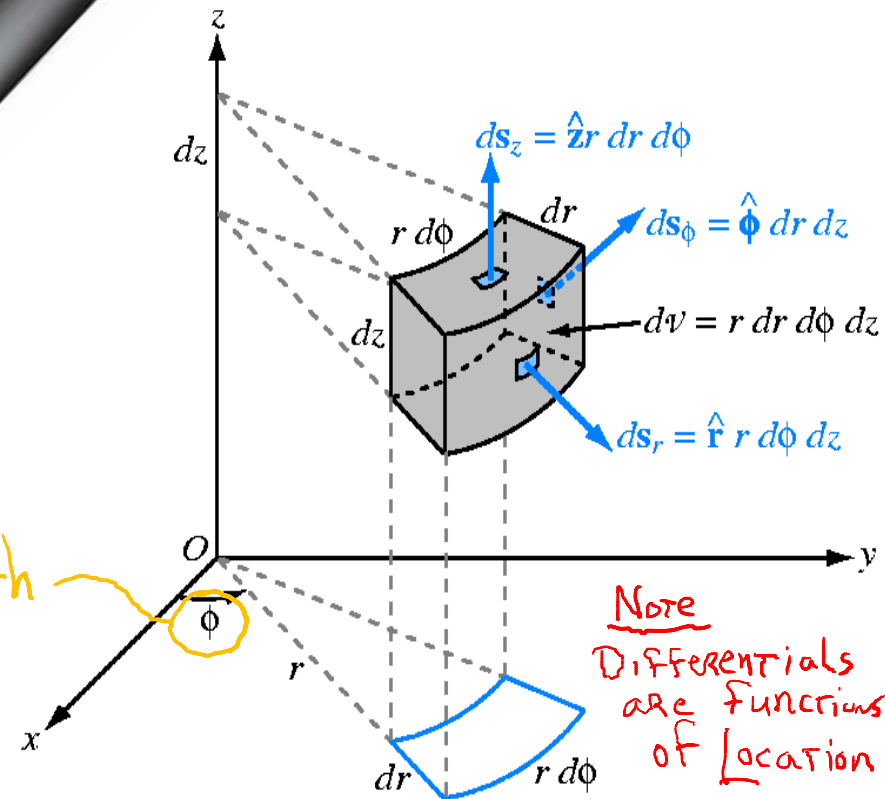
Orthogonal Basis Set  
(Cylindrical Coords)

•  $\hat{r}$  &  $\hat{\phi}$  are functions of  $\phi$  !

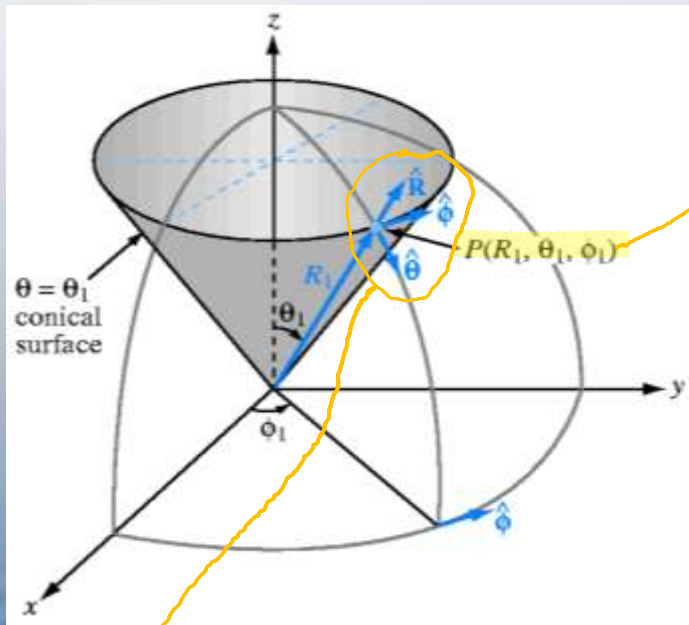
• What is  $\hat{z} \times \hat{r}$ , etc.?



Azimuth



Note  
Differentials are functions of location

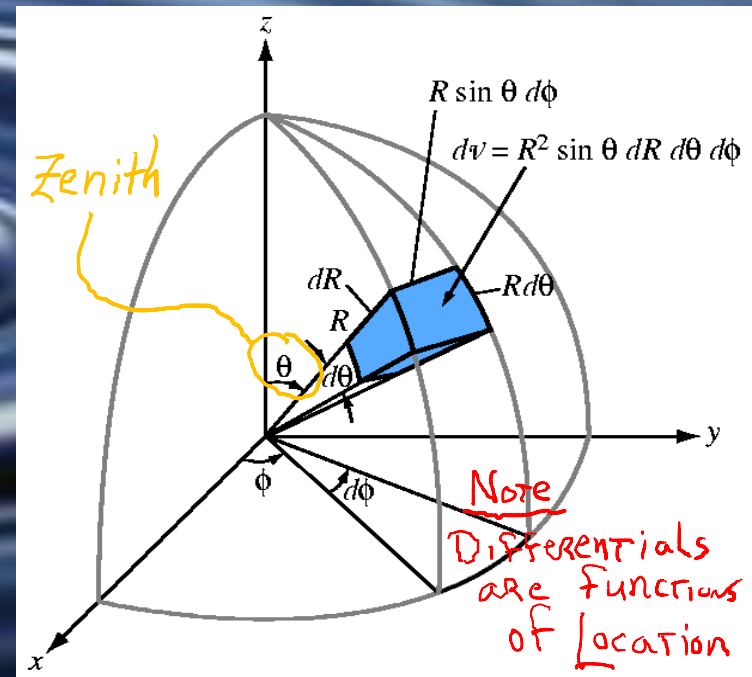


position



ortho basis  
(spherical)

• All 3 depend  
on  $\phi$  and  $\theta$



	Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
Coordinate variables	$x, y, z$	$r, \phi, z$	$R, \theta, \phi$
Vector representation, $\mathbf{A} =$	$\hat{\mathbf{x}}A_x + \hat{\mathbf{y}}A_y + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{r}}A_r + \hat{\boldsymbol{\phi}}A_\phi + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{R}}A_R + \hat{\boldsymbol{\theta}}A_\theta + \hat{\boldsymbol{\phi}}A_\phi$
Magnitude of $\mathbf{A}$ , $ \mathbf{A}  =$	$\sqrt{A_x^2 + A_y^2 + A_z^2}$	$\sqrt{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt{A_R^2 + A_\theta^2 + A_\phi^2}$
Position vector $\overrightarrow{OP_L} =$	$\hat{\mathbf{x}}x_L + \hat{\mathbf{y}}y_L + \hat{\mathbf{z}}z_L,$ for $P(x_L, y_L, z_L)$	$\hat{\mathbf{r}}r_L + \hat{\mathbf{z}}z_L,$ for $P(r_L, \phi_L, z_L)$	$\hat{\mathbf{R}}R_L,$ for $P(R_L, \theta_L, \phi_L)$
Base vectors properties	$\hat{\mathbf{x}} \cdot \hat{\mathbf{x}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1$ $\hat{\mathbf{x}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{z}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{x}} = 0$ $\hat{\mathbf{x}} \times \hat{\mathbf{y}} = \hat{\mathbf{z}}$ $\hat{\mathbf{y}} \times \hat{\mathbf{z}} = \hat{\mathbf{x}}$ $\hat{\mathbf{z}} \times \hat{\mathbf{x}} = \hat{\mathbf{y}}$	$\hat{\mathbf{r}} \cdot \hat{\mathbf{r}} = \hat{\boldsymbol{\phi}} \cdot \hat{\boldsymbol{\phi}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1$ $\hat{\mathbf{r}} \cdot \hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}} \cdot \hat{\mathbf{z}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{r}} = 0$ $\hat{\mathbf{r}} \times \hat{\boldsymbol{\phi}} = \hat{\mathbf{z}}$ $\hat{\boldsymbol{\phi}} \times \hat{\mathbf{z}} = \hat{\mathbf{r}}$ $\hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\boldsymbol{\phi}}$	$\hat{\mathbf{R}} \cdot \hat{\mathbf{R}} = \hat{\boldsymbol{\theta}} \cdot \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\phi}} \cdot \hat{\boldsymbol{\phi}} = 1$ $\hat{\mathbf{R}} \cdot \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\theta}} \cdot \hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}} \cdot \hat{\mathbf{R}} = 0$ $\hat{\mathbf{R}} \times \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\phi}}$ $\hat{\boldsymbol{\theta}} \times \hat{\boldsymbol{\phi}} = \hat{\mathbf{R}}$ $\hat{\boldsymbol{\phi}} \times \hat{\mathbf{R}} = \hat{\boldsymbol{\theta}}$
Dot product, $\mathbf{A} \cdot \mathbf{B} =$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\phi B_\phi + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
Cross product, $\mathbf{A} \times \mathbf{B} =$	$\begin{vmatrix} \hat{\mathbf{x}} & \hat{\mathbf{y}} & \hat{\mathbf{z}} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{r}} & \hat{\boldsymbol{\phi}} & \hat{\mathbf{z}} \\ A_r & A_\phi & A_z \\ B_r & B_\phi & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{R}} & \hat{\boldsymbol{\theta}} & \hat{\boldsymbol{\phi}} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
Differential length, $d\mathbf{l} =$	$\hat{\mathbf{x}}dx + \hat{\mathbf{y}}dy + \hat{\mathbf{z}}dz$	$\hat{\mathbf{r}}dr + \hat{\boldsymbol{\phi}}r d\phi + \hat{\mathbf{z}}dz$	$\hat{\mathbf{R}}dR + \hat{\boldsymbol{\theta}}R d\theta + \hat{\boldsymbol{\phi}}R \sin\theta d\phi$
Differential surface areas	$ds_x = \hat{\mathbf{x}}dydz$ $ds_y = \hat{\mathbf{y}}dxdz$ $ds_z = \hat{\mathbf{z}}dxdy$	$ds_r = \hat{\mathbf{r}}r d\phi dz$ $ds_\phi = \hat{\boldsymbol{\phi}}dr dz$ $ds_z = \hat{\mathbf{z}}r dr d\phi$	$ds_R = \hat{\mathbf{R}}R^2 \sin\theta d\theta d\phi$ $ds_\theta = \hat{\boldsymbol{\theta}}R \sin\theta dR d\phi$ $ds_\phi = \hat{\boldsymbol{\phi}}R dR d\theta$
Differential volume, $dV =$	$dxdydz$	$rdr d\phi dz$	$R^2 \sin\theta dR d\theta d\phi$

**Problem 3.22** Use the appropriate expression for the differential surface area  $ds$  to

determine the area of each of the following surfaces:

(a)  $r = 3; 0 \leq \phi \leq \pi/3; -2 \leq z \leq 2,$

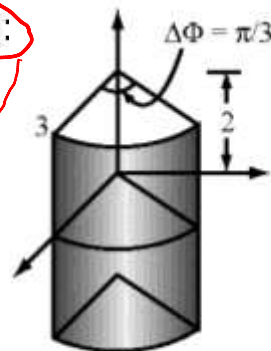
(b)  $2 \leq r \leq 5; \pi/2 \leq \phi \leq \pi; z = 0,$

(c)  $2 \leq r \leq 5; \phi = \pi/4; -2 \leq z \leq 2,$

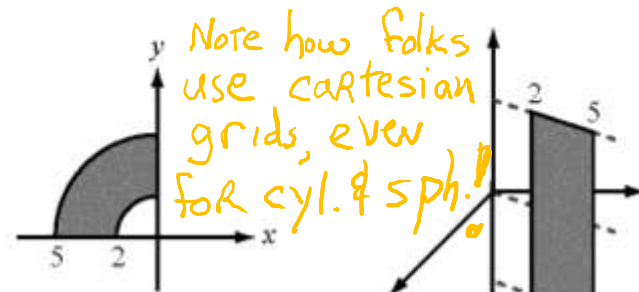
(d)  $R = 2; 0 \leq \theta \leq \pi/3; 0 \leq \phi \leq \pi,$

(e)  $0 \leq R \leq 5; \theta = \pi/3; 0 \leq \phi \leq 2\pi.$

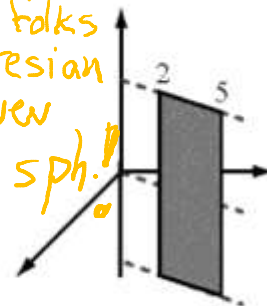
Also sketch the outlines of each of the surfaces.



(a)



(b)



(c)

(a) Using Eq. (3.43a),

$$A = \int_{z=-2}^2 \int_{\phi=0}^{\pi/3} (r)|_{r=3} d\phi dz = \left( (3\phi z) \Big|_{\phi=0}^{\pi/3} \right) \Big|_{z=-2}^2 = 4\pi.$$

(b) Using Eq. (3.43c),

$$A = \int_{r=2}^5 \int_{\phi=\pi/2}^{\pi} (r)|_{z=0} d\phi dr = \left( \left( \frac{1}{2} r^2 \phi \right) \Big|_{r=2}^5 \right) \Big|_{\phi=\pi/2}^{\pi} = \frac{21\pi}{4}.$$

(c) Using Eq. (3.43b),

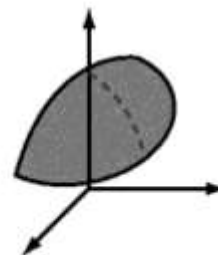
$$A = \int_{z=-2}^2 \int_{r=2}^5 (1)|_{\phi=\pi/4} dr dz = \left( (rz) \Big|_{z=-2}^2 \right) \Big|_{r=2}^5 = 12.$$

(d) Using Eq. (3.50b),

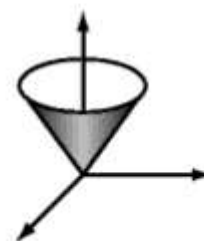
$$A = \int_{\theta=0}^{\pi/3} \int_{\phi=0}^{\pi} (R^2 \sin \theta) \Big|_{R=2} d\phi d\theta = \left( (-4\phi \cos \theta) \Big|_{\theta=0}^{\pi/3} \right) \Big|_{\phi=0}^{\pi} = 2\pi.$$

(e) Using Eq. (3.50c),

$$A = \int_{R=0}^5 \int_{\phi=0}^{2\pi} (R \sin \theta) \Big|_{\theta=\pi/3} d\phi dR = \left( \left( \frac{1}{2} R^2 \phi \sin \frac{\pi}{3} \right) \Big|_{\phi=0}^{2\pi} \right) \Big|_{R=0}^5 = \frac{25\sqrt{3}\pi}{2}.$$



(d)



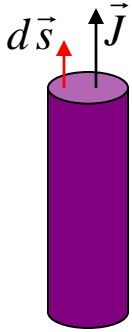
(e)

Note how folks use cartesian grids, even for cyl. & sph.!



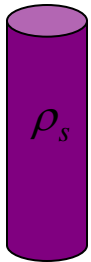
### Examples:

Find the total current flowing through a copper wire that has a circular cross-section with radius  $r_0 = 1$  mm. The current density is  $J = 10$  mA/mm<sup>2</sup>.



$$\begin{aligned} I &= \int_S \vec{J} \cdot d\vec{s} = \int_{\phi=0}^{2\pi} \int_{r=0}^{r_0} J r dr d\phi = 2\pi J \int_{r=0}^{r_0} r dr = 2\pi J \left( \frac{r^2}{2} \right)_0^{r_0} = 2\pi J \frac{r_0^2}{2} = \\ &= 2\pi \times 10^4 \times \frac{0.001^2}{2} = 31.4 \text{ mA} \end{aligned}$$

Find the total electric charge on the surface of a plastic rod if the surface charge density is  $\rho_s = 2$  pC/m<sup>2</sup>. The radius of the rod is  $r_0 = 5$  mm and its length is  $l = 10$  cm.



$$\begin{aligned} Q &= \int_S \rho_s ds = \int_{S_{cylinder}} \rho_s ds + 2 \times \left( \int_{S_{top}} \rho_s ds \right) = \int_{z=0}^l \int_{\phi=0}^{2\pi} \rho_s r_0 d\phi dz + 2 \times \int_{\phi=0}^{2\pi} \int_{r=0}^{r_0} \rho_s r dr d\phi = \\ &= 2\pi \rho_s r_0 (z)_0^l + 2 \times 2\pi \rho_s \left( \frac{r^2}{2} \right)_0^{r_0} = 2\pi \rho_s r_0 l + 4\pi \rho_s \frac{r_0^2}{2} = 2\pi \rho_s r_0 (l + r_0) \\ &= 2\pi \times 2 \times 10^{-9} \times 0.005 \times (0.1 + 0.005) = 6.6 \text{ pC} \end{aligned}$$

**Problem 3.26** At a given point in space, vectors **A** and **B** are given in spherical coordinates by

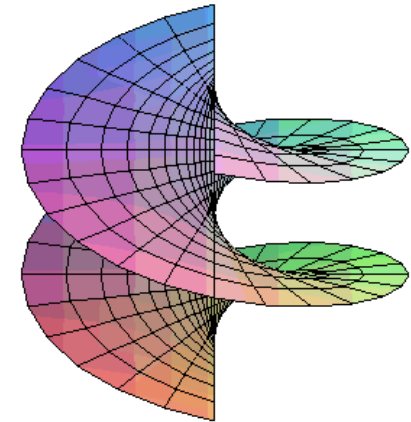
$t = -3.1416$

$$\mathbf{A} = \hat{\mathbf{R}}4 + \hat{\boldsymbol{\theta}}2 - \hat{\boldsymbol{\phi}},$$

$$\mathbf{B} = -\hat{\mathbf{R}}2 + \hat{\boldsymbol{\phi}}3.$$

Find:

- (a) the scalar component, or projection, of **B** in the direction of **A**,
- (b) the vector component of **B** in the direction of **A**,
- (c) the vector component of **B** perpendicular to **A**.



(a) Scalar component of **B** in direction of **A**:

$$\begin{aligned} C = \mathbf{B} \cdot \hat{\mathbf{a}} &= \mathbf{B} \cdot \frac{\mathbf{A}}{|\mathbf{A}|} = (-\hat{\mathbf{R}}2 + \hat{\boldsymbol{\phi}}3) \cdot \frac{(\hat{\mathbf{R}}4 + \hat{\boldsymbol{\theta}}2 - \hat{\boldsymbol{\phi}})}{\sqrt{16 + 4 + 1}} \\ &= \frac{-8 - 3}{\sqrt{21}} = -\frac{11}{\sqrt{21}} = -2.4. \end{aligned}$$

(b) Vector component of **B** in direction of **A**:

$$\begin{aligned} \mathbf{C} = \hat{\mathbf{a}}C &= \mathbf{A} \frac{C}{|\mathbf{A}|} = (\hat{\mathbf{R}}4 + \hat{\boldsymbol{\theta}}2 - \hat{\boldsymbol{\phi}}) \frac{(-2.4)}{\sqrt{21}} \\ &= -(\hat{\mathbf{R}}2.09 + \hat{\boldsymbol{\theta}}1.05 - \hat{\boldsymbol{\phi}}0.52). \end{aligned}$$

(c) Vector component of **B** perpendicular to **A**:

$$\begin{aligned} \mathbf{D} = \mathbf{B} - \mathbf{C} &= (-\hat{\mathbf{R}}2 + \hat{\boldsymbol{\phi}}3) + (\hat{\mathbf{R}}2.09 + \hat{\boldsymbol{\theta}}1.05 - \hat{\boldsymbol{\phi}}0.52) \\ &= \hat{\mathbf{R}}0.09 + \hat{\boldsymbol{\theta}}1.05 + \hat{\boldsymbol{\phi}}2.48. \end{aligned}$$

**Problem 3.18** Use arrows to sketch each of the following vector fields:

(a)  $\mathbf{E}_1 = \hat{\mathbf{x}}x - \hat{\mathbf{y}}y$ ,

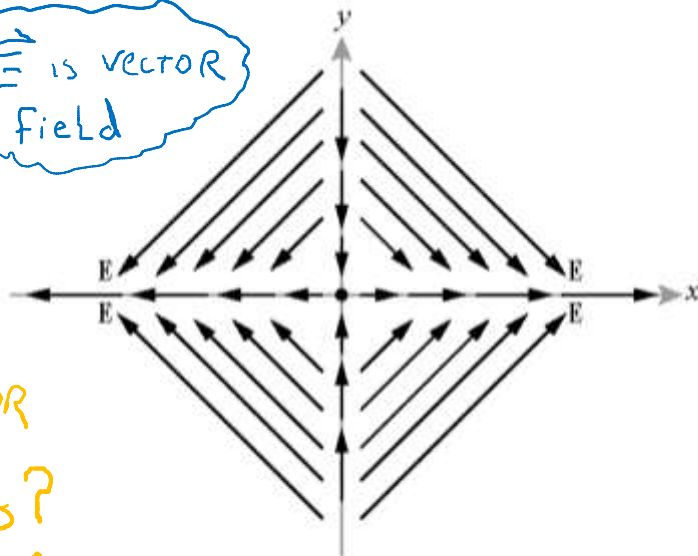
(b)  $\mathbf{E}_2 = -\hat{\boldsymbol{\phi}}$ ,

(c)  $\mathbf{E}_3 = \hat{\mathbf{y}} \frac{1}{x}$ ,

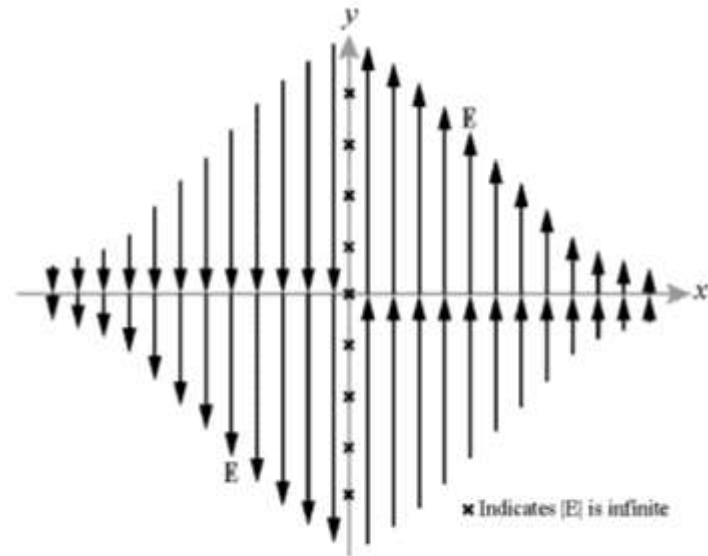
(d)  $\mathbf{E}_4 = \hat{\mathbf{r}} \cos \phi$ .

$\vec{E}$  is vector field

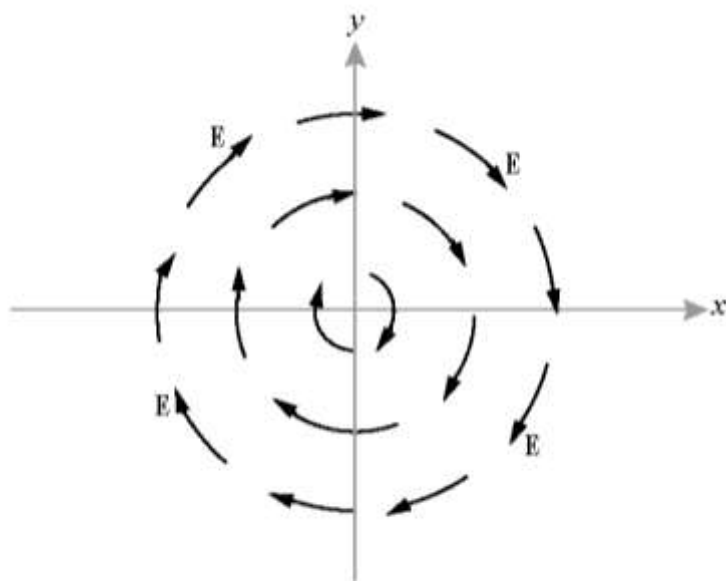
are these  
in rectangular,  
cylindrical, or  
spherical  
coordinates?



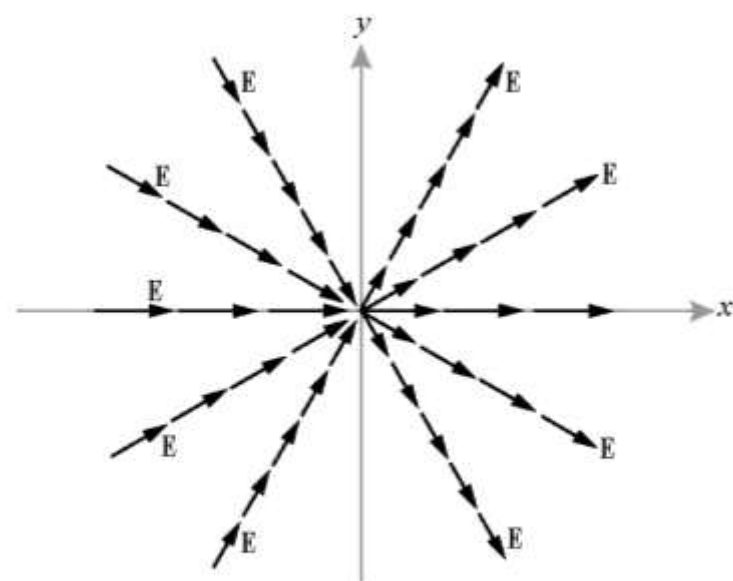
P2.14a:  $\mathbf{E}_1 = \hat{\mathbf{x}}x - \hat{\mathbf{y}}y$



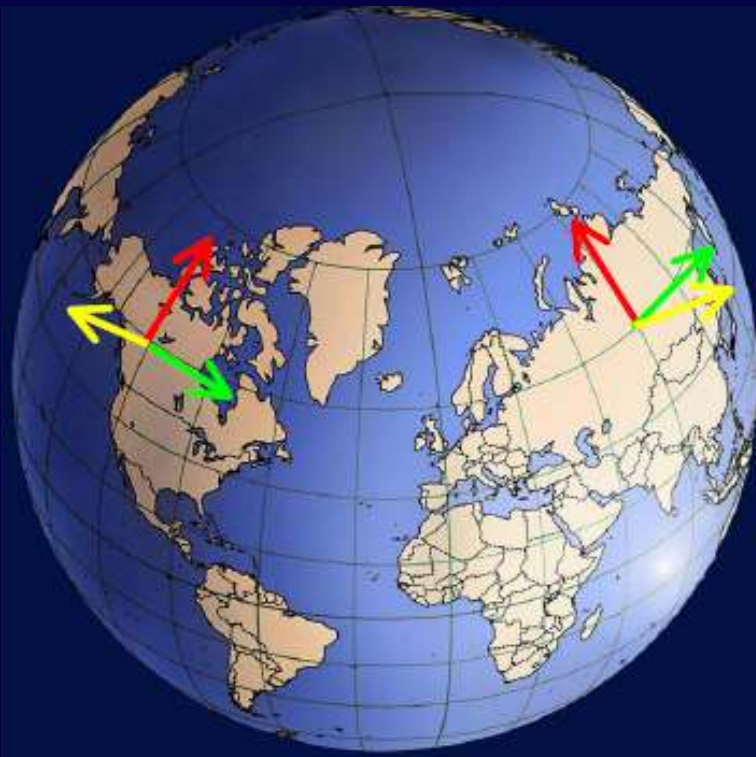
P2.14c:  $\mathbf{E}_3 = \hat{\mathbf{y}}(1/x)$



P2.14b:  $\mathbf{E}_2 = -\hat{\boldsymbol{\phi}}$



P2.14d:  $\mathbf{E}_4 = \hat{\mathbf{r}} \cos \phi$

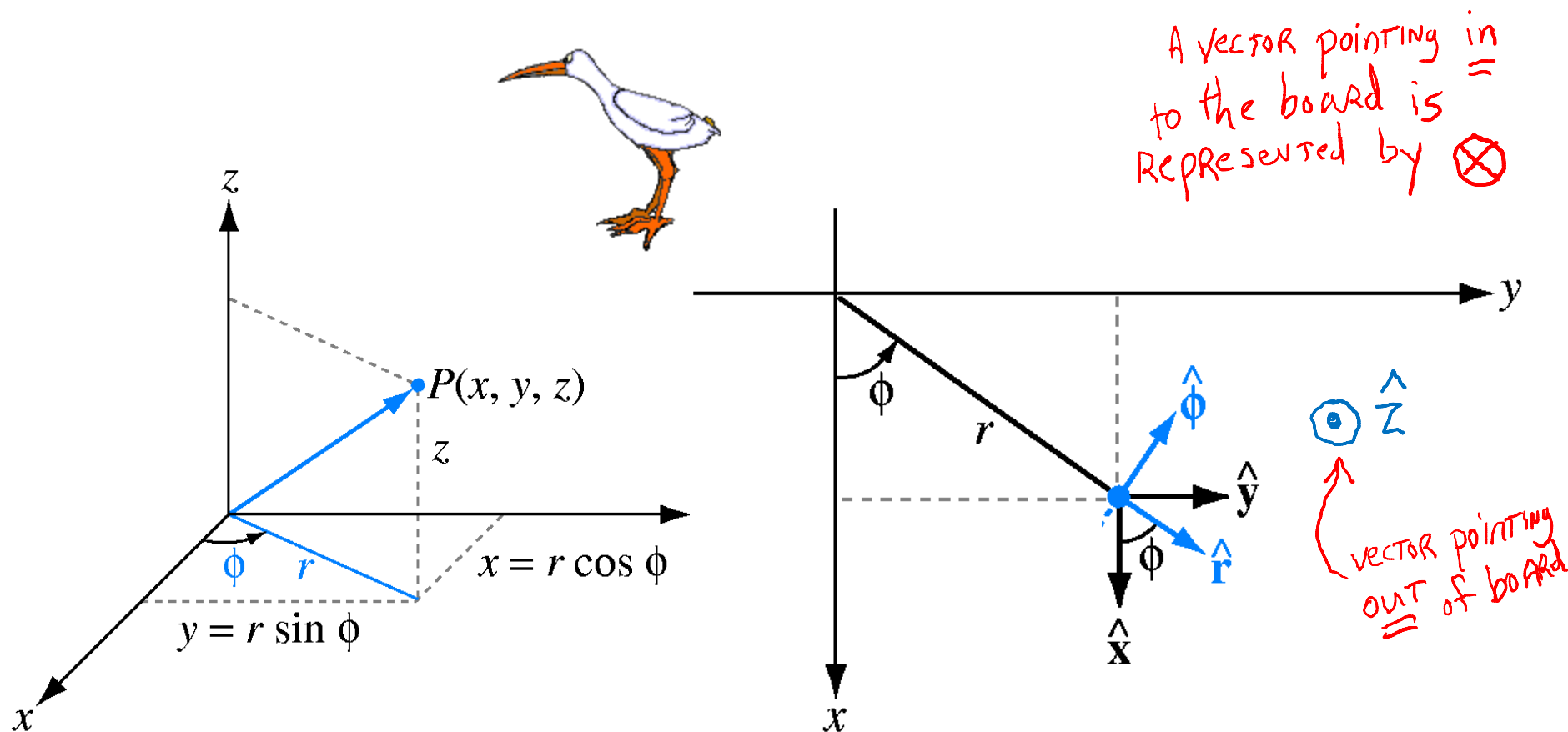


Position coordinates are *different* from basis vectors, and so are their conversion between coordinate systems.  
(you likely experienced the *former* in previous courses ☺)

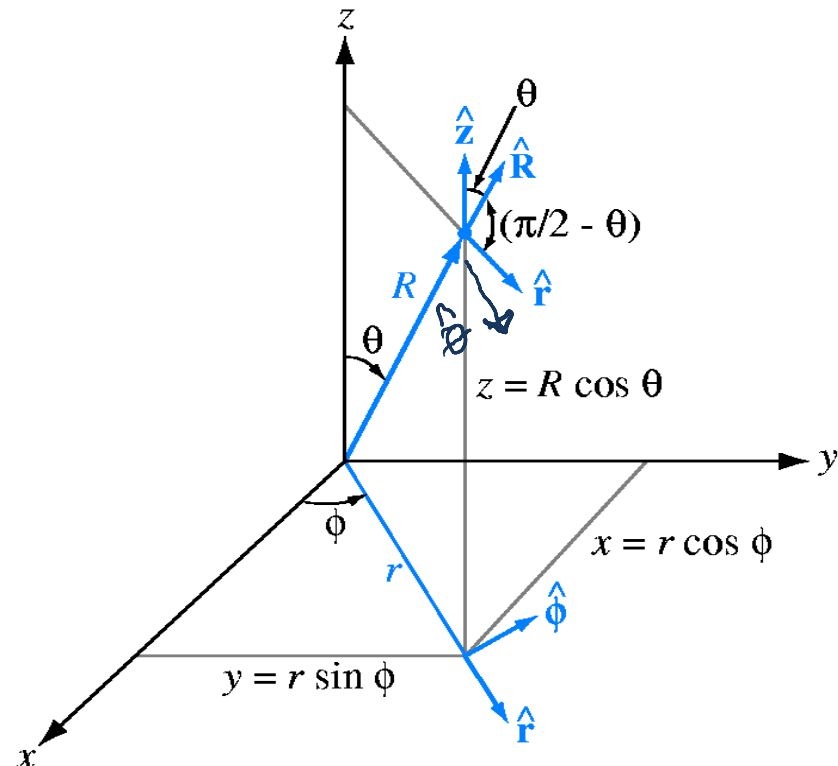
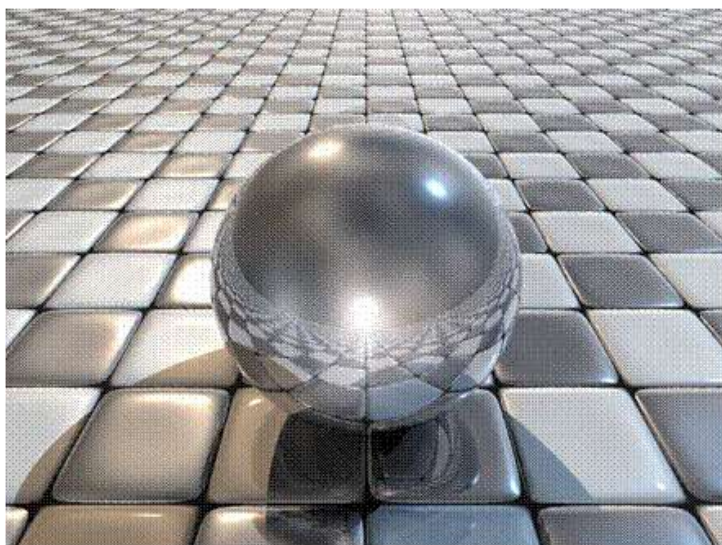
Distance between points is most “easily” calculated in the Cartesian (a.k.a Rectangular) coordinate system.

	Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
Coordinate variables	$x, y, z$	$r, \phi, z$	$R, \theta, \phi$
Vector representation, $\mathbf{A} =$	$\hat{\mathbf{x}}A_x + \hat{\mathbf{y}}A_y + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{r}}A_r + \hat{\boldsymbol{\phi}}A_\phi + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{R}}A_R + \hat{\boldsymbol{\theta}}A_\theta + \hat{\boldsymbol{\phi}}A_\phi$
Magnitude of $\mathbf{A}$ , $ \mathbf{A}  =$	$\sqrt{A_x^2 + A_y^2 + A_z^2}$	$\sqrt{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt{A_R^2 + A_\theta^2 + A_\phi^2}$
Position vector $\overrightarrow{OP_l} =$	$\hat{\mathbf{x}}x_l + \hat{\mathbf{y}}y_l + \hat{\mathbf{z}}z_l$ , for $P(x_l, y_l, z_l)$	$\hat{\mathbf{r}}r_l + \hat{\mathbf{z}}z_l$ , for $P(r_l, \phi_l, z_l)$	$\hat{\mathbf{R}}R_l$ , for $P(R_l, \theta_l, \phi_l)$
Base vectors properties	$\hat{\mathbf{x}} \cdot \hat{\mathbf{x}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1$ $\hat{\mathbf{x}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{z}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{x}} = 0$ $\hat{\mathbf{x}} \times \hat{\mathbf{y}} = \hat{\mathbf{z}}$ $\hat{\mathbf{y}} \times \hat{\mathbf{z}} = \hat{\mathbf{x}}$ $\hat{\mathbf{z}} \times \hat{\mathbf{x}} = \hat{\mathbf{y}}$	$\hat{\mathbf{r}} \cdot \hat{\mathbf{r}} = \hat{\boldsymbol{\phi}} \cdot \hat{\boldsymbol{\phi}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1$ $\hat{\mathbf{r}} \cdot \hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}} \cdot \hat{\mathbf{z}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{r}} = 0$ $\hat{\mathbf{r}} \times \hat{\boldsymbol{\phi}} = \hat{\mathbf{z}}$ $\hat{\boldsymbol{\phi}} \times \hat{\mathbf{z}} = \hat{\mathbf{r}}$ $\hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\boldsymbol{\phi}}$	$\hat{\mathbf{R}} \cdot \hat{\mathbf{R}} = \hat{\boldsymbol{\theta}} \cdot \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\phi}} \cdot \hat{\boldsymbol{\phi}} = 1$ $\hat{\mathbf{R}} \cdot \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\theta}} \cdot \hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}} \cdot \hat{\mathbf{R}} = 0$ $\hat{\mathbf{R}} \times \hat{\boldsymbol{\theta}} = \hat{\boldsymbol{\phi}}$ $\hat{\boldsymbol{\theta}} \times \hat{\boldsymbol{\phi}} = \hat{\mathbf{R}}$ $\hat{\boldsymbol{\phi}} \times \hat{\mathbf{R}} = \hat{\boldsymbol{\theta}}$
Dot product, $\mathbf{A} \cdot \mathbf{B} =$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\phi B_\phi + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
Cross product, $\mathbf{A} \times \mathbf{B} =$	$\begin{vmatrix} \hat{\mathbf{x}} & \hat{\mathbf{y}} & \hat{\mathbf{z}} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{r}} & \hat{\boldsymbol{\phi}} & \hat{\mathbf{z}} \\ A_r & A_\phi & A_z \\ B_r & B_\phi & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{R}} & \hat{\boldsymbol{\theta}} & \hat{\boldsymbol{\phi}} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
Differential length, $d\mathbf{l} =$	$\hat{\mathbf{x}}dx + \hat{\mathbf{y}}dy + \hat{\mathbf{z}}dz$	$\hat{\mathbf{r}}dr + \hat{\boldsymbol{\phi}}r d\phi + \hat{\mathbf{z}}dz$	$\hat{\mathbf{R}}dR + \hat{\boldsymbol{\theta}}R d\theta + \hat{\boldsymbol{\phi}}R \sin \theta d\phi$
Differential surface areas	$ds_x = \hat{\mathbf{x}}dydz$ $ds_y = \hat{\mathbf{y}}dxdz$ $ds_z = \hat{\mathbf{z}}dxdy$	$ds_r = \hat{\mathbf{r}}r d\phi dz$ $ds_\phi = \hat{\boldsymbol{\phi}}dr dz$ $ds_z = \hat{\mathbf{z}}r dr d\phi$	$ds_R = \hat{\mathbf{R}}R^2 \sin \theta d\theta d\phi$ $ds_\theta = \hat{\boldsymbol{\theta}}R \sin \theta dR d\phi$ $ds_\phi = \hat{\boldsymbol{\phi}}R dR d\theta$
Differential volume, $d\mathcal{V} =$	$dxdydz$	$r dr d\phi dz$	$R^2 \sin \theta dR d\theta d\phi$





Transformation	Coordinate Variables	Unit Vectors	Vector Components
Cartesian to cylindrical	$r = \sqrt{x^2 + y^2}$ $\phi = \tan^{-1}(y/x)$ $z = z$	$\hat{r} = \hat{x} \cos \phi + \hat{y} \sin \phi$ $\hat{\phi} = -\hat{x} \sin \phi + \hat{y} \cos \phi$ $\hat{z} = \hat{z}$	$A_r = A_x \cos \phi + A_y \sin \phi$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$ $A_z = A_z$
Cylindrical to Cartesian	$x = r \cos \phi$ $y = r \sin \phi$ $z = z$	$\hat{x} = \hat{r} \cos \phi - \hat{\phi} \sin \phi$ $\hat{y} = \hat{r} \sin \phi + \hat{\phi} \cos \phi$ $\hat{z} = \hat{z}$	$A_x = A_r \cos \phi - A_\phi \sin \phi$ $A_y = A_r \sin \phi + A_\phi \cos \phi$ $A_z = A_z$



Transformation	Coordinate Variables	Unit Vectors	Vector Components
<b>Cartesian to spherical</b>	$R = \sqrt[3]{x^2 + y^2 + z^2}$ $\theta = \tan^{-1}[\sqrt{x^2 + y^2}/z]$ $\phi = \tan^{-1}(y/x)$	$\hat{\mathbf{R}} = \hat{\mathbf{x}} \sin \theta \cos \phi + \hat{\mathbf{y}} \sin \theta \sin \phi + \hat{\mathbf{z}} \cos \theta$ $\hat{\boldsymbol{\theta}} = \hat{\mathbf{x}} \cos \theta \cos \phi + \hat{\mathbf{y}} \cos \theta \sin \phi - \hat{\mathbf{z}} \sin \theta$ $\hat{\boldsymbol{\phi}} = -\hat{\mathbf{x}} \sin \phi + \hat{\mathbf{y}} \cos \phi$	$A_R = A_x \sin \theta \cos \phi + A_y \sin \theta \sin \phi + A_z \cos \theta$ $A_\theta = A_x \cos \theta \cos \phi + A_y \cos \theta \sin \phi - A_z \sin \theta$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$
<b>Spherical to Cartesian</b>	$x = R \sin \theta \cos \phi$ $y = R \sin \theta \sin \phi$ $z = R \cos \theta$	$\hat{\mathbf{x}} = \hat{\mathbf{R}} \sin \theta \cos \phi + \hat{\boldsymbol{\theta}} \cos \theta \cos \phi - \hat{\boldsymbol{\phi}} \sin \phi$ $\hat{\mathbf{y}} = \hat{\mathbf{R}} \sin \theta \sin \phi + \hat{\boldsymbol{\theta}} \cos \theta \sin \phi + \hat{\boldsymbol{\phi}} \cos \phi$ $\hat{\mathbf{z}} = \hat{\mathbf{R}} \cos \theta - \hat{\boldsymbol{\theta}} \sin \theta$	$A_x = A_R \sin \theta \cos \phi + A_\theta \cos \theta \cos \phi - A_\phi \sin \phi$ $A_y = A_R \sin \theta \sin \phi + A_\theta \cos \theta \sin \phi + A_\phi \cos \phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$

Transformation	Coordinate Variables	Unit Vectors	Vector Components
Cylindrical to spherical	$R = \sqrt{r^2 + z^2}$ $\theta = \tan^{-1}(r/z)$ $\phi = \phi$	$\hat{\mathbf{R}} = \hat{\mathbf{r}} \sin \theta + \hat{\mathbf{z}} \cos \theta$ $\hat{\boldsymbol{\theta}} = \hat{\mathbf{r}} \cos \theta - \hat{\mathbf{z}} \sin \theta$ $\hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}}$	$A_R = A_r \sin \theta + A_z \cos \theta$ $A_{\theta} = A_r \cos \theta - A_z \sin \theta$ $A_{\phi} = A_{\phi}$
Spherical to cylindrical	$r = R \sin \theta$ $\phi = \phi$ $z = R \cos \theta$	$\hat{\mathbf{r}} = \hat{\mathbf{R}} \sin \theta + \hat{\boldsymbol{\theta}} \cos \theta$ $\hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}}$ $\hat{\mathbf{z}} = \hat{\mathbf{R}} \cos \theta - \hat{\boldsymbol{\theta}} \sin \theta$	$A_r = A_R \sin \theta + A_{\theta} \cos \theta$ $A_{\phi} = A_{\phi}$ $A_z = A_R \cos \theta - A_{\theta} \sin \theta$

*Might* not need these all too often...

...however, you will learn some additional field operators next:

\* **Gradient** (for scalar fields)



\* **Divergence** (for vector fields)



\* **Curl** (for vector fields)



**Problem 3.30** Transform the following vectors into cylindrical coordinates and then evaluate them at the indicated points:

(a)  $\mathbf{A} = \hat{\mathbf{x}}(x+y)$  at  $P_1(1, 2, 3)$ ,

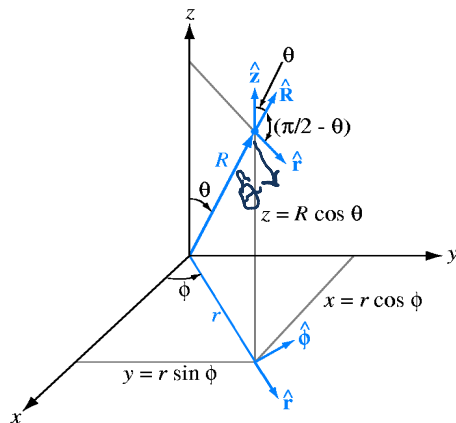
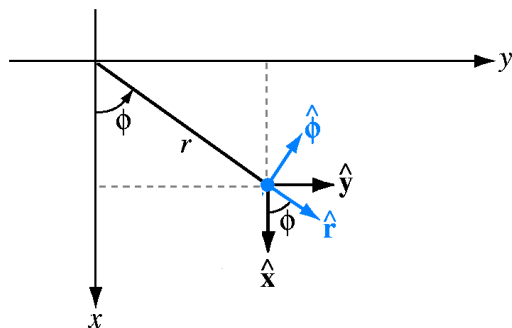
(b)  $\mathbf{B} = \hat{\mathbf{x}}(y-x) + \hat{\mathbf{y}}(x-y)$  at  $P_2(1, 0, 2)$ ,

(c)  $\mathbf{C} = \hat{\mathbf{x}}y^2/(x^2+y^2) - \hat{\mathbf{y}}x^2/(x^2+y^2) + \hat{\mathbf{z}}4$  at  $P_3(1, -1, 2)$ ,

(d)  $\mathbf{D} = \hat{\mathbf{R}}\sin\theta + \hat{\boldsymbol{\theta}}\cos\theta + \hat{\boldsymbol{\phi}}\cos^2\phi$  at  $P_4(2, \pi/2, \pi/4)$ ,

(e)  $\mathbf{E} = \hat{\mathbf{R}}\cos\phi + \hat{\boldsymbol{\theta}}\sin\phi + \hat{\boldsymbol{\phi}}\sin^2\theta$  at  $P_5(3, \pi/2, \pi)$ .

what coord. system are we starting in??



(a)

$$\mathbf{A} = (\hat{\mathbf{r}}\cos\phi - \hat{\boldsymbol{\phi}}\sin\phi)(r\cos\phi + r\sin\phi) = \hat{\mathbf{r}}r\cos\phi(\cos\phi + \sin\phi) - \hat{\boldsymbol{\phi}}r\sin\phi(\cos\phi + \sin\phi),$$

$$P_1 = (\sqrt{1^2 + 2^2}, \tan^{-1}(2/1), 3) = (\sqrt{5}, 63.4^\circ, 3),$$

$$\mathbf{A}(P_1) = (\hat{\mathbf{r}}0.447 - \hat{\boldsymbol{\phi}}0.894)\sqrt{5}(.447 + .894) = \hat{\mathbf{r}}1.34 - \hat{\boldsymbol{\phi}}2.68.$$

(b)

$$\mathbf{B} = (\hat{\mathbf{r}}\cos\phi - \hat{\boldsymbol{\phi}}\sin\phi)(r\sin\phi - r\cos\phi) + (\hat{\boldsymbol{\phi}}\cos\phi + \hat{\mathbf{r}}\sin\phi)(r\cos\phi - r\sin\phi) = \hat{\mathbf{r}}r(2\sin\phi\cos\phi - 1) + \hat{\boldsymbol{\phi}}r(\cos^2\phi - \sin^2\phi) = \hat{\mathbf{r}}r(\sin 2\phi - 1) + \hat{\boldsymbol{\phi}}r\cos 2\phi,$$

$$P_2 = (\sqrt{1^2 + 0^2}, \tan^{-1}(0/1), 2) = (1, 0^\circ, 2),$$

$$\mathbf{B}(P_2) = -\hat{\mathbf{r}} + \hat{\boldsymbol{\phi}}.$$

(c)

$$\mathbf{C} = (\hat{\mathbf{r}}\cos\phi - \hat{\boldsymbol{\phi}}\sin\phi)\frac{r^2\sin^2\phi}{r^2} - (\hat{\boldsymbol{\phi}}\cos\phi + \hat{\mathbf{r}}\sin\phi)\frac{r^2\cos^2\phi}{r^2} + \hat{\mathbf{z}}4 = \hat{\mathbf{r}}\sin\phi\cos\phi(\sin\phi - \cos\phi) - \hat{\boldsymbol{\phi}}(\sin^3\phi + \cos^3\phi) + \hat{\mathbf{z}}4,$$

$$P_3 = (\sqrt{1^2 + (-1)^2}, \tan^{-1}(-1/1), 2) = (\sqrt{2}, -45^\circ, 2),$$

$$\mathbf{C}(P_3) = \hat{\mathbf{r}}0.707 + \hat{\mathbf{z}}4.$$

(d)

$$\mathbf{D} = (\hat{\mathbf{r}}\sin\theta + \hat{\mathbf{z}}\cos\theta)\sin\theta + (\hat{\mathbf{r}}\cos\theta - \hat{\mathbf{z}}\sin\theta)\cos\theta + \hat{\boldsymbol{\phi}}\cos^2\phi = \hat{\mathbf{r}} + \hat{\boldsymbol{\phi}}\cos^2\phi,$$

$$P_4 = (2\sin(\pi/2), \pi/4, 2\cos(\pi/2)) = (2, 45^\circ, 0),$$

$$\mathbf{D}(P_4) = \hat{\mathbf{r}} + \hat{\boldsymbol{\phi}}\frac{1}{2}.$$

(e)

$$\mathbf{E} = (\hat{\mathbf{r}}\sin\theta + \hat{\mathbf{z}}\cos\theta)\cos\phi + (\hat{\mathbf{r}}\cos\theta - \hat{\mathbf{z}}\sin\theta)\sin\phi + \hat{\boldsymbol{\phi}}\sin^2\theta,$$

$$P_5 = \left(3, \frac{\pi}{2}, \pi\right),$$

$$\mathbf{E}(P_5) = \left(\hat{\mathbf{r}}\sin\frac{\pi}{2} + \hat{\mathbf{z}}\cos\frac{\pi}{2}\right)\cos\pi + \left(\hat{\mathbf{r}}\cos\frac{\pi}{2} - \hat{\mathbf{z}}\sin\frac{\pi}{2}\right)\sin\pi + \hat{\boldsymbol{\phi}}\sin^2\frac{\pi}{2} = -\hat{\mathbf{r}} + \hat{\boldsymbol{\phi}}.$$

Transformation	Coordinate Variables	Unit Vectors	Vector Components
Cartesian to cylindrical	$r = \sqrt{x^2 + y^2}$ $\phi = \tan^{-1}(y/x)$ $z = z$	$\hat{\mathbf{r}} = \hat{\mathbf{x}}\cos\phi + \hat{\mathbf{y}}\sin\phi$ $\hat{\boldsymbol{\phi}} = -\hat{\mathbf{x}}\sin\phi + \hat{\mathbf{y}}\cos\phi$ $\hat{\mathbf{z}} = \hat{\mathbf{z}}$	$A_r = A_x\cos\phi + A_y\sin\phi$ $A_\phi = -A_x\sin\phi + A_y\cos\phi$ $A_z = A_z$
Spherical to cylindrical	$r = R\sin\theta$ $\phi = \phi$ $z = R\cos\theta$	$\hat{\mathbf{r}} = \hat{\mathbf{R}}\sin\theta + \hat{\boldsymbol{\theta}}\cos\theta$ $\hat{\boldsymbol{\phi}} = \hat{\boldsymbol{\phi}}$ $\hat{\mathbf{z}} = \hat{\mathbf{R}}\cos\theta - \hat{\boldsymbol{\theta}}\sin\theta$	$A_r = A_R\sin\theta + A_\theta\cos\theta$ $A_\phi = A_\phi$ $A_z = A_R\cos\theta - A_\theta\sin\theta$

# T-Line Example...

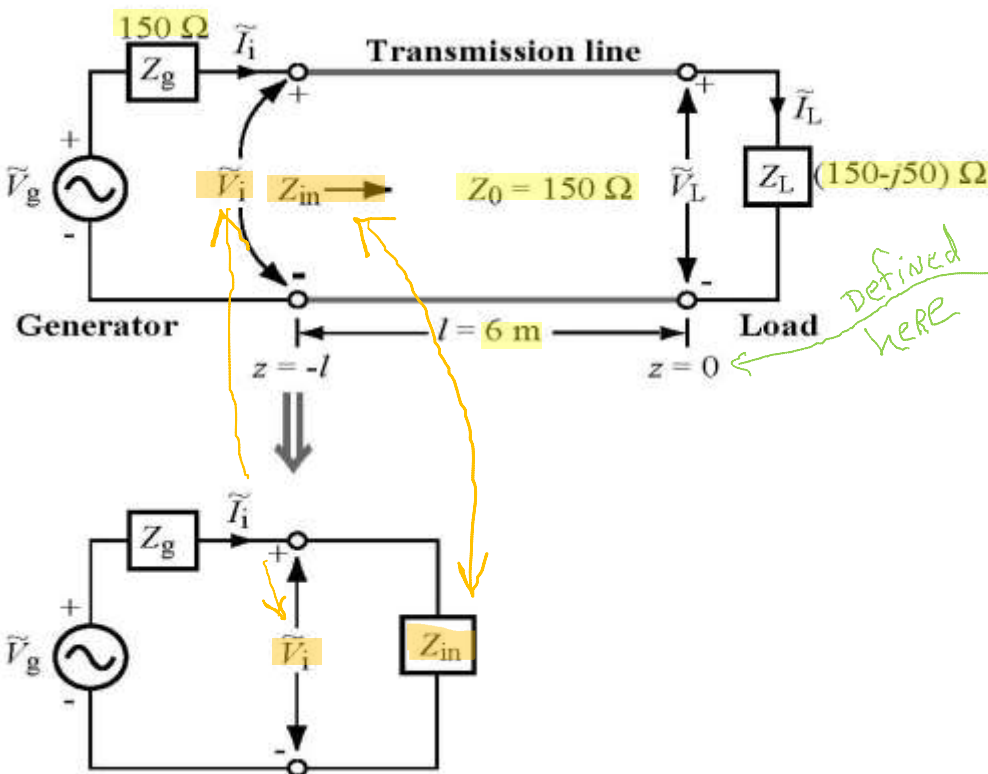
**Problem 2.22** A 6-m section of 150-Ω lossless line is driven by a source with

$$v_g(t) = 5 \cos(8\pi \times 10^7 t - 30^\circ) \text{ (V)}$$

and  $Z_g = 150 \Omega$ . If the line, which has a relative permittivity  $\epsilon_r = 2.25$ , is terminated in a load  $Z_L = (150 - j50) \Omega$ , find

- $\lambda$  on the line,
- the reflection coefficient at the load,
- the input impedance,
- the input voltage  $\tilde{V}_i$ ,
- the time-domain input voltage  $v_i(t)$ .

$\Rightarrow 2\pi F$   
 $\Rightarrow F = 40 \text{ MHz}$



**Solution:**

$$v_g(t) = 5 \cos(8\pi \times 10^7 t - 30^\circ) \text{ V,}$$

$$\tilde{V}_g = 5e^{-j30^\circ} \text{ V.}$$

(a)

$$u_p = \frac{c}{\sqrt{\epsilon_r}} = \frac{3 \times 10^8}{\sqrt{2.25}} = 2 \times 10^8 \text{ (m/s),}$$

$$\lambda = \frac{u_p}{f} = \frac{2\pi u_p}{\omega} = \frac{2\pi \times 2 \times 10^8}{8\pi \times 10^7} = 5 \text{ m,}$$

$$\beta = \frac{\omega}{u_p} = \frac{8\pi \times 10^7}{2 \times 10^8} = 0.4\pi \text{ (rad/m),}$$

$$\beta l = 0.4\pi \times 6 = 2.4\pi \text{ (rad).}$$

more on ER Later 😊

$$\Rightarrow l = 1.2 \lambda$$

can only get away with this when it's lossless

Since this exceeds  $2\pi$  (rad), we can subtract  $2\pi$ , which leaves a remainder  $\beta l = 0.4\pi$  (rad).

$$(b) \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{150 - j50 - 150}{150 - j50 + 150} = \frac{-j50}{300 - j50} = 0.16e^{-j80.54^\circ}.$$

(c)

$$Z_{in} = Z_0 \left[ \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right]$$

$$= 150 \left[ \frac{(150 - j50) + j1 \frac{\tan(0.4\pi)}{\tan(0.4\pi)}}{150 + j(150 - j50) \tan(0.4\pi)} \right] = (115.70 + j27.42) \Omega.$$

(d)

$$\tilde{V}_i = \frac{\tilde{V}_g Z_{in}}{Z_g + Z_{in}} = \frac{5e^{-j30^\circ} (115.7 + j27.42)}{150 + 115.7 + j27.42}$$

$$= 5e^{-j30^\circ} \left( \frac{115.7 + j27.42}{265.7 + j27.42} \right)$$

$$= 5e^{-j30^\circ} \times 0.44e^{j7.44^\circ} = 2.2e^{-j22.56^\circ} \text{ (V).}$$

Phasors and Voltage Dividers

(e)

$$v_i(t) = \Re\{\tilde{V}_i e^{j\omega t}\} = \Re\{2.2e^{-j22.56^\circ} e^{j\omega t}\} = 2.2 \cos(8\pi \times 10^7 t - 22.56^\circ) \text{ V.}$$

Phasors back to time domain

“Mathematics is the art of giving the same name to different things.”

**-J. H. Poincare**

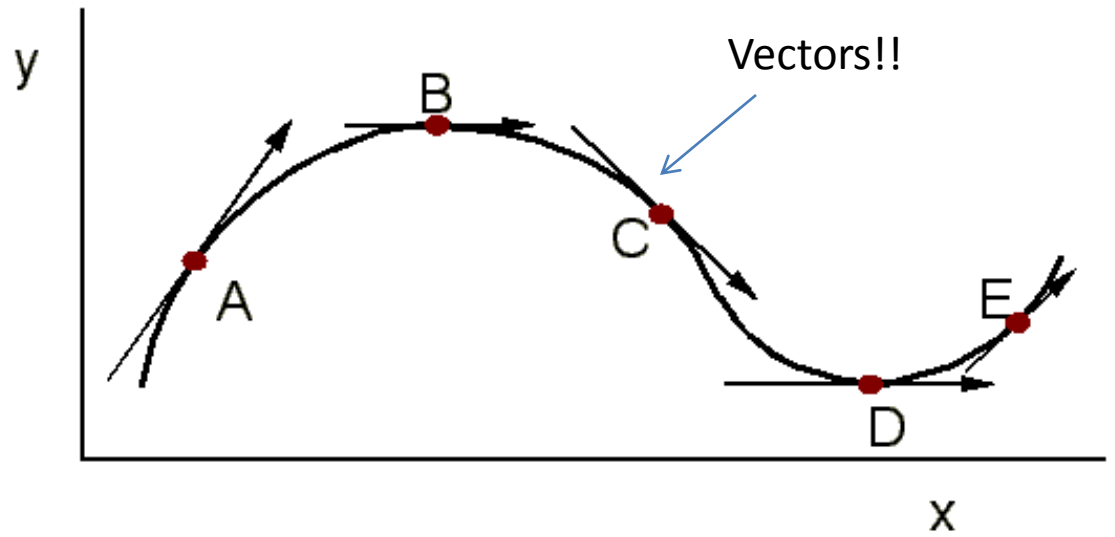
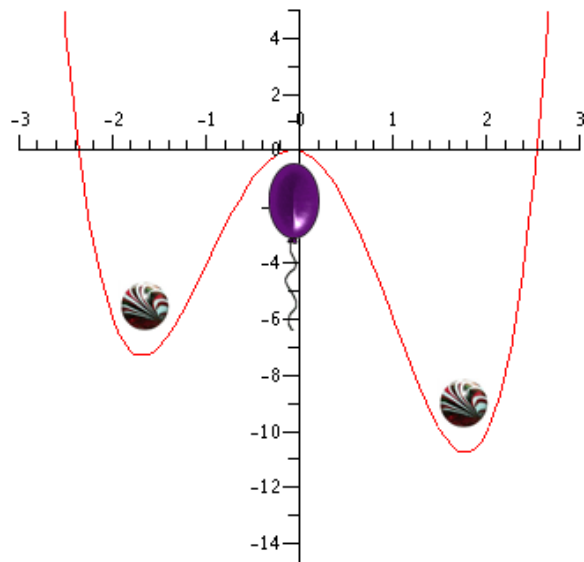
[http://en.wikipedia.org/wiki/  
Henri\\_Poincar%C3%A9](http://en.wikipedia.org/wiki/Henri_Poincar%C3%A9)

"Mathematics is a game played according to certain simple rules with meaningless marks on paper.“

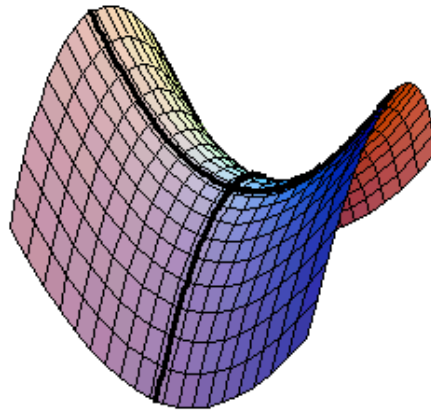
**- David Hilbert**

[http://en.wikipedia.org/wiki/David\\_Hilbert](http://en.wikipedia.org/wiki/David_Hilbert)

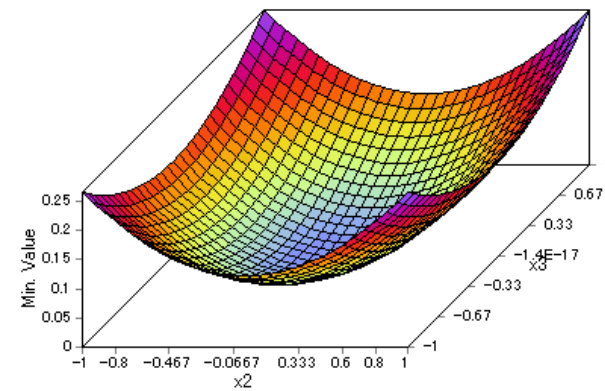




2-D



3-D





# Gradient

- Max/Min
- Optimization
- Physical “flows”

# del operator

$$\nabla \equiv \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

Cartesian

other...

$$\nabla V = \hat{r} \frac{\partial V}{\partial r} + \hat{\phi} \frac{1}{r} \frac{\partial V}{\partial \phi} + \hat{z} \frac{\partial V}{\partial z}$$

$$\nabla V = \hat{R} \frac{\partial V}{\partial R} + \hat{\theta} \frac{1}{R} \frac{\partial V}{\partial \theta} + \hat{\phi} \frac{1}{R \sin \theta} \frac{\partial V}{\partial \phi}$$

## Gradient

scalar field  
 $V(x, y, z)$

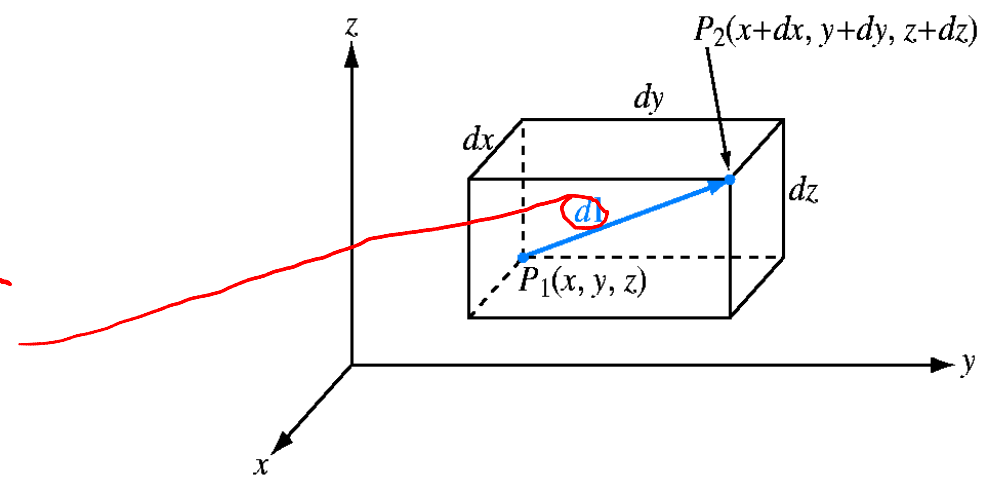
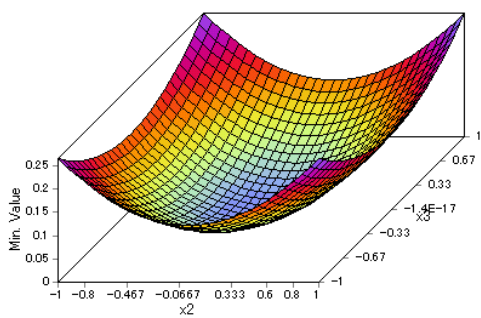
$$\Rightarrow \text{grad } V \equiv \nabla V = \hat{x} \frac{\partial V}{\partial x} + \hat{y} \frac{\partial V}{\partial y} + \hat{z} \frac{\partial V}{\partial z}$$

vector field

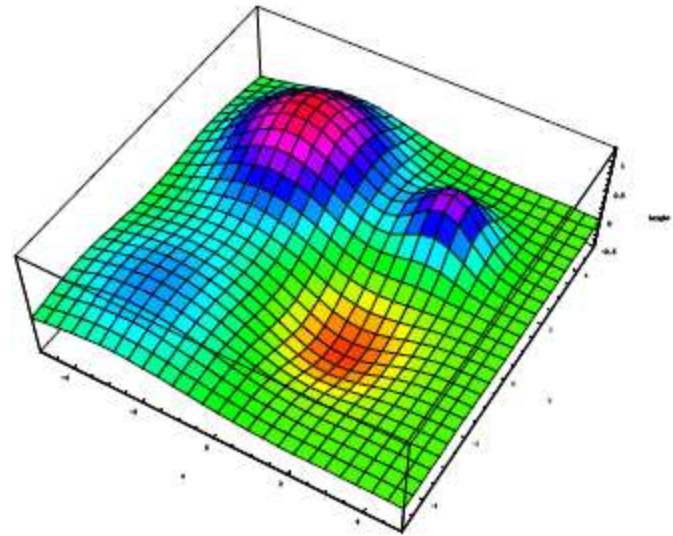
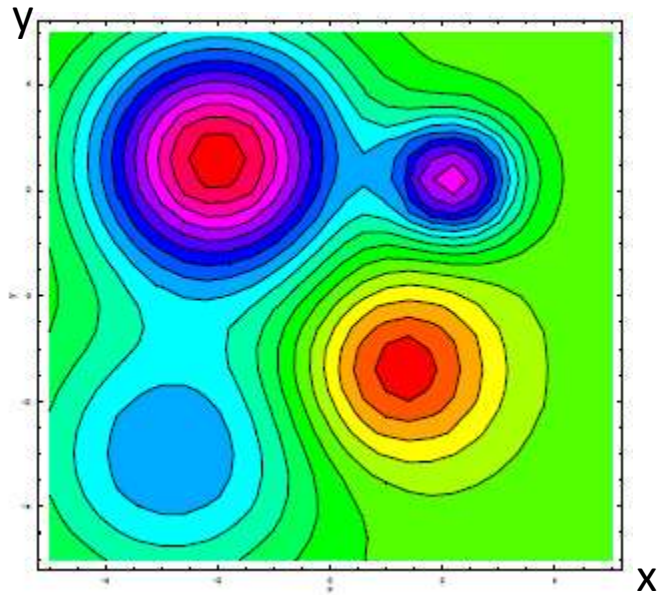
## Directional Derivative

$$\frac{\partial V}{\partial l} = \nabla V \cdot \hat{a}_l$$

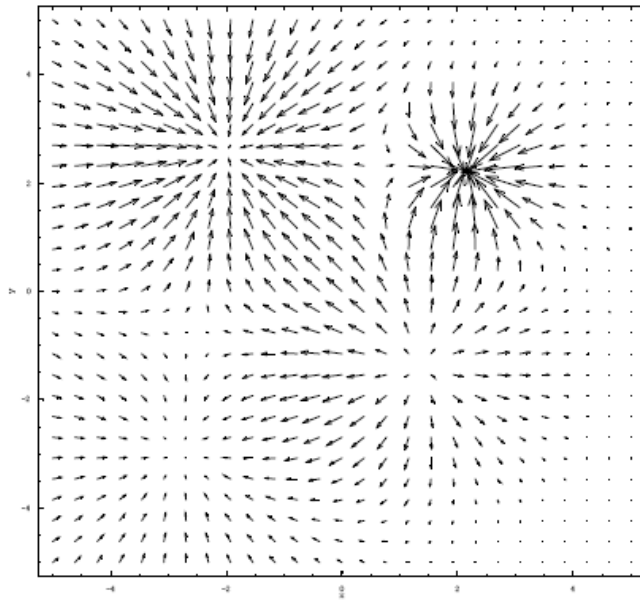
unit vector  
of  $d\vec{l}$



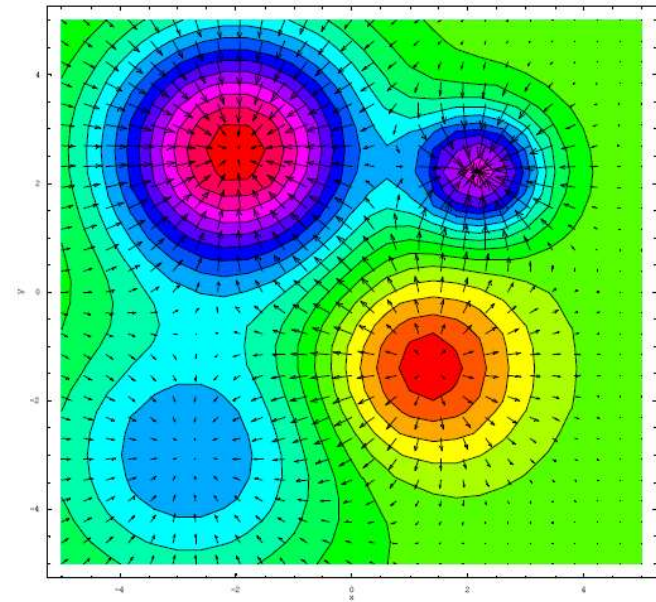
Height,  $h(x,y)$  ... a scalar field



Gradient of  $h(x,y)$ ,  $\nabla h(x,y)$  ... a vector field



Overlay



**Problem 3.32** Find the **gradient** of the following **scalar** functions:

(a)  $T = 3/(x^2 + z^2),$

(b)  $V = xy^2z^4,$

(c)  $U = z \cos \phi / (1 + r^2),$

(d)  $W = e^{-R} \sin \theta,$

(e)  $S = 4x^2 e^{-z} + y^3,$

(f)  $N = r^2 \cos^2 \phi,$

(g)  $M = R \cos \theta \sin \phi.$

(a) From Eq. (3.72),

$$\nabla T = -\hat{\mathbf{x}} \frac{6x}{(x^2 + z^2)^2} - \hat{\mathbf{z}} \frac{6z}{(x^2 + z^2)^2}.$$

(b) From Eq. (3.72),

$$\nabla V = \hat{\mathbf{x}} y^2 z^4 + \hat{\mathbf{y}} 2xyz^4 + \hat{\mathbf{z}} 4xy^2 z^3.$$

(c) From Eq. (3.82),

$$\nabla U = -\hat{\mathbf{r}} \frac{2rz \cos \phi}{(1 + r^2)^2} - \hat{\phi} \frac{z \sin \phi}{r(1 + r^2)} + \hat{\mathbf{z}} \frac{\cos \phi}{1 + r^2}.$$

(d) From Eq. (3.83),

$$\nabla W = -\hat{\mathbf{R}} e^{-R} \sin \theta + \hat{\theta} (e^{-R}/R) \cos \theta.$$

(e) From Eq. (3.72),

$$S = 4x^2 e^{-z} + y^3,$$

$$\nabla S = \hat{\mathbf{x}} \frac{\partial S}{\partial x} + \hat{\mathbf{y}} \frac{\partial S}{\partial y} + \hat{\mathbf{z}} \frac{\partial S}{\partial z} = \hat{\mathbf{x}} 8x e^{-z} + \hat{\mathbf{y}} 3y^2 - \hat{\mathbf{z}} 4x^2 e^{-z}.$$

(f) From Eq. (3.82),

$$N = r^2 \cos^2 \phi,$$

$$\nabla N = \hat{\mathbf{r}} \frac{\partial N}{\partial r} + \hat{\phi} \frac{1}{r} \frac{\partial N}{\partial \phi} + \hat{\mathbf{z}} \frac{\partial N}{\partial z} = \hat{\mathbf{r}} 2r \cos^2 \phi - \hat{\phi} 2r \sin \phi \cos \phi.$$

(g) From Eq. (3.83),

$$M = R \cos \theta \sin \phi,$$

$$\nabla M = \hat{\mathbf{R}} \frac{\partial M}{\partial R} + \hat{\theta} \frac{1}{R} \frac{\partial M}{\partial \theta} + \hat{\phi} \frac{1}{R \sin \theta} \frac{\partial M}{\partial \phi} = \hat{\mathbf{R}} \cos \theta \sin \phi - \hat{\theta} \sin \theta \sin \phi + \hat{\phi} \frac{\cos \phi}{\tan \theta}.$$

Figure out your coordinate system!!

$$\nabla V = \hat{\mathbf{x}} \frac{\partial V}{\partial x} + \hat{\mathbf{y}} \frac{\partial V}{\partial y} + \hat{\mathbf{z}} \frac{\partial V}{\partial z}$$

$$\nabla V = \hat{\mathbf{r}} \frac{\partial V}{\partial r} + \hat{\phi} \frac{1}{r} \frac{\partial V}{\partial \phi} + \hat{\mathbf{z}} \frac{\partial V}{\partial z}$$

$$\nabla V = \hat{\mathbf{R}} \frac{\partial V}{\partial R} + \hat{\theta} \frac{1}{R} \frac{\partial V}{\partial \theta} + \hat{\phi} \frac{1}{R \sin \theta} \frac{\partial V}{\partial \phi}$$

**Problem 3.36** For the scalar function  $T = \frac{1}{2}e^{-r/5} \cos \phi$ , determine its **directional derivative** along the radial direction  $\hat{\mathbf{r}}$  and then evaluate it at  $P(2, \pi/4, 3)$ .

$$T = \frac{1}{2}e^{-r/5} \cos \phi,$$

$$\nabla T = \hat{\mathbf{r}} \frac{\partial T}{\partial r} + \hat{\boldsymbol{\phi}} \frac{1}{r} \frac{\partial T}{\partial \phi} + \hat{\mathbf{z}} \frac{\partial T}{\partial z} = -\hat{\mathbf{r}} \frac{e^{-r/5} \cos \phi}{10} - \hat{\boldsymbol{\phi}} \frac{e^{-r/5} \sin \phi}{2r},$$

$$\frac{dT}{dl} = \nabla T \cdot \hat{\mathbf{r}} = -\frac{e^{-r/5} \cos \phi}{10},$$

$$\left. \frac{dT}{dl} \right|_{(2, \pi/4, 3)} = -\frac{e^{-2/5} \cos \frac{\pi}{4}}{10} = -4.74 \times 10^{-2}.$$

Directional Derivative  
in  $\hat{\mathbf{r}}$  direction.

Cylindrical

Example:

Find the gradient of the scalar field  $a = a_0 e^{-x} \sin(\pi y)$  and determine its value at  $(1, 2, 0)$ .

$$\begin{aligned} \nabla a &= \hat{\mathbf{x}} \frac{\partial a}{\partial x} + \hat{\mathbf{y}} \frac{\partial a}{\partial y} + \hat{\mathbf{z}} \frac{\partial a}{\partial z} = \\ &= -\hat{\mathbf{x}} a_0 e^{-x} \sin(\pi y) + \hat{\mathbf{y}} \pi a_0 e^{-x} \cos(\pi y) = \\ &= [-\hat{\mathbf{x}} \sin(\pi y) + \hat{\mathbf{y}} \pi \cos(\pi y)] a_0 e^{-x} \end{aligned}$$

$$\nabla a(1, 2, 0) = [-\hat{\mathbf{x}} \sin(2\pi) + \hat{\mathbf{y}} \pi \cos(2\pi)] a_0 e^{-1} = \hat{\mathbf{y}} \frac{a_0 \pi}{e}$$

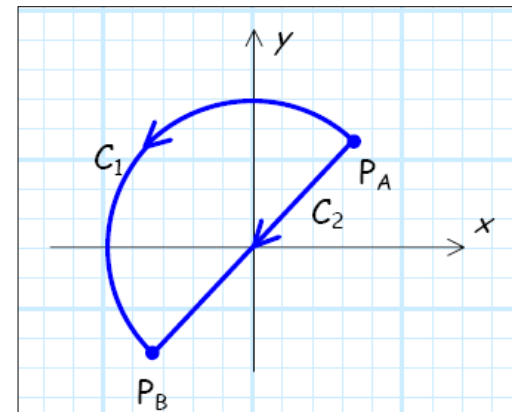
# Conservative Field

1. A conservative vector field can always be expressed as the **gradient** of a **scalar** field.
2. The gradient of **any** scalar field is therefore a conservative vector field.

$$\mathbf{C}(\bar{\mathbf{r}}) = \nabla g(\bar{\mathbf{r}})$$

## 2.5 Not all vector fields are conservative!!

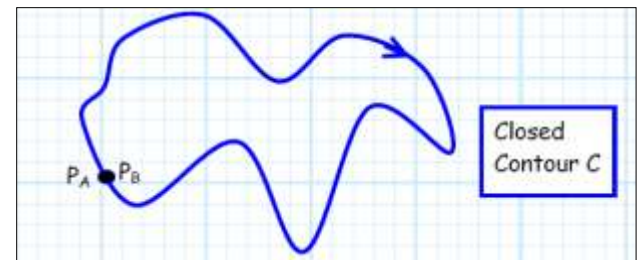
3. Integration over an **open** contour is dependent **only** on the value of scalar field  $g(\bar{\mathbf{r}})$  at the beginning and ending points of the contour (i.e., integration is **path independent**).



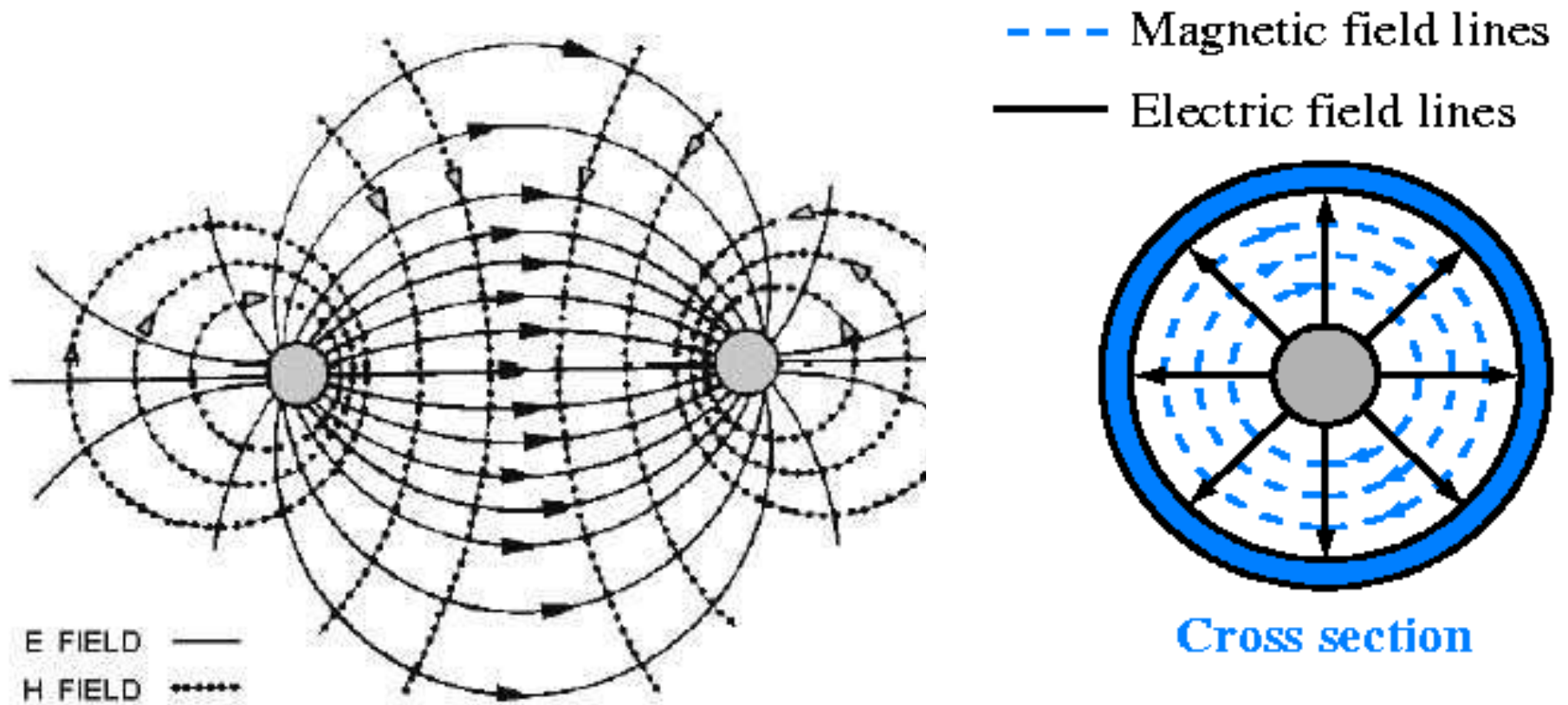
$$\begin{aligned}\int_C \mathbf{C}(\bar{\mathbf{r}}) \cdot d\bar{\ell} &= \int_C \nabla g(\bar{\mathbf{r}}) \cdot d\bar{\ell} \\ &= g(\bar{\mathbf{r}} = \bar{\mathbf{r}}_A) - g(\bar{\mathbf{r}} = \bar{\mathbf{r}}_B)\end{aligned}$$

## 3.5 Path integration is fun ???!

4. Integration of a conservative vector field over any **closed** contour is always equal to **zero**.





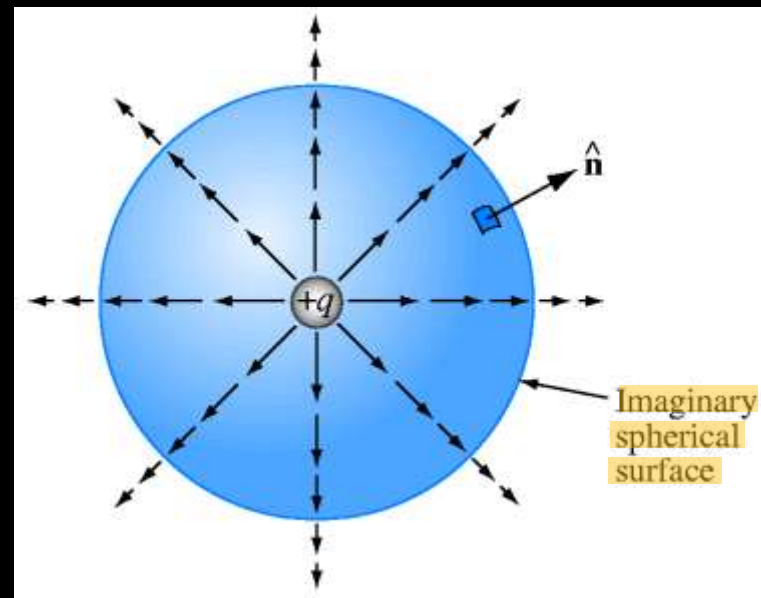
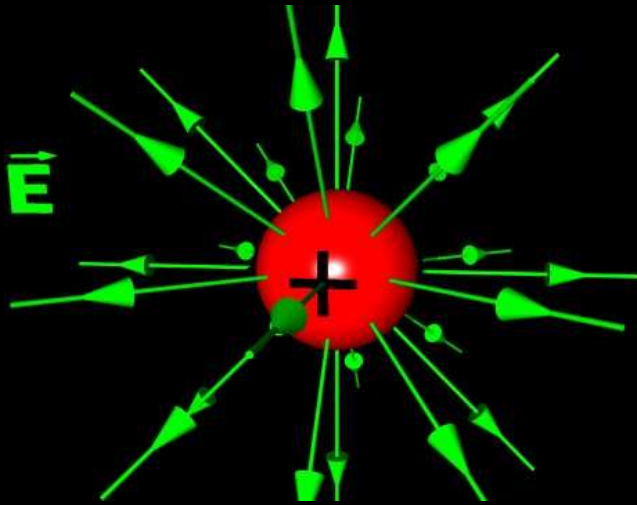


$$\vec{E} = -\nabla V \quad \Rightarrow \quad \nabla \times \vec{E} = \nabla \times (-\nabla V) = 0$$

$$V_{21} = V_2 - V_1 = - \int_{P_1}^{P_2} \vec{E} \cdot d\vec{l}$$



# Electric Field

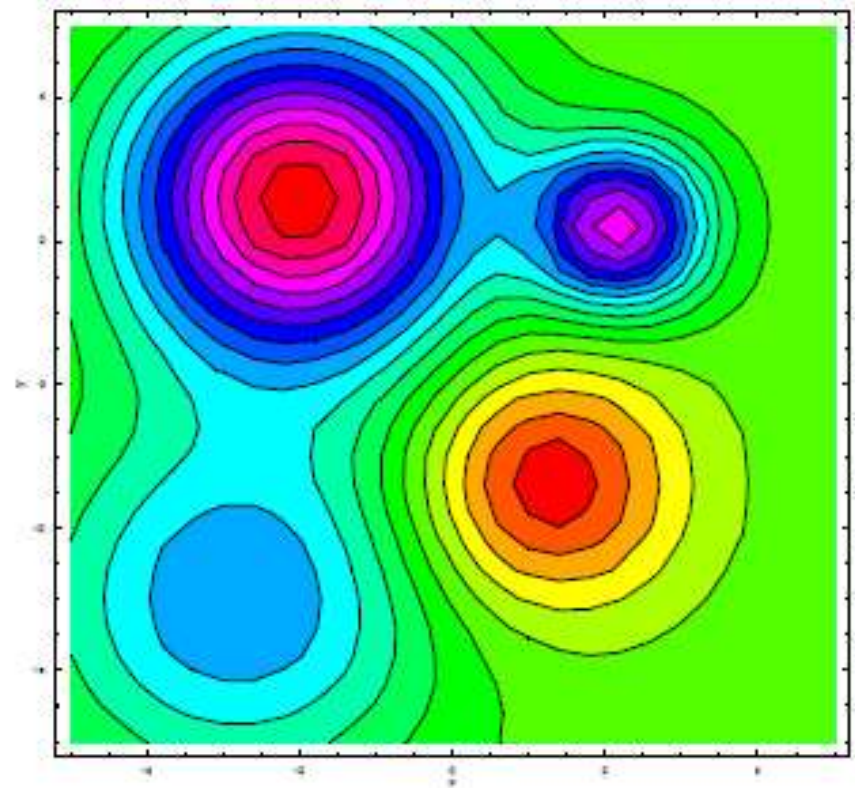
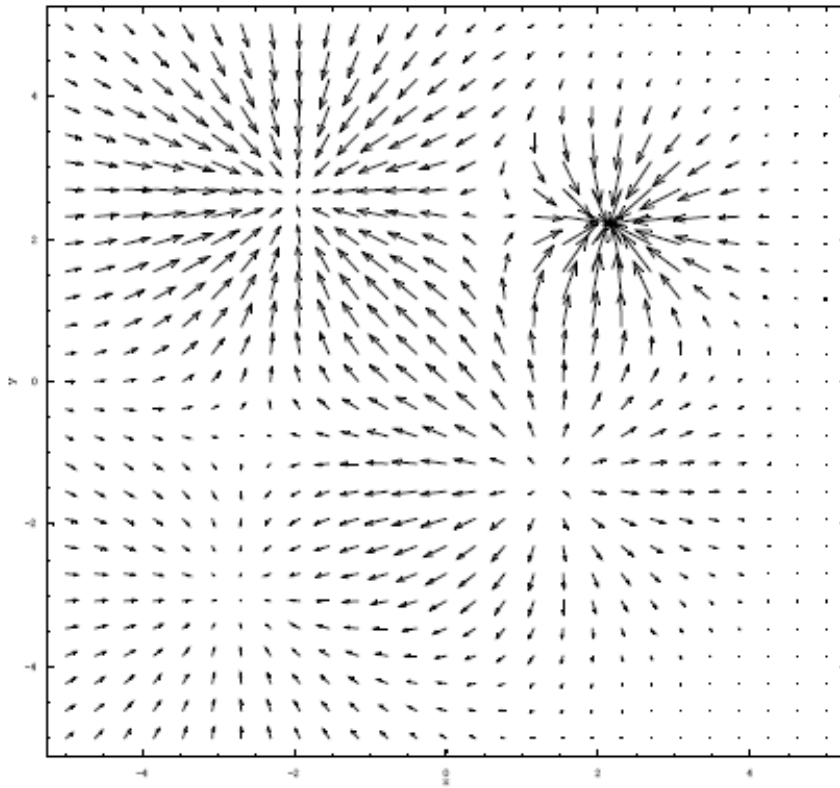


The mathematical definition of **divergence** is:

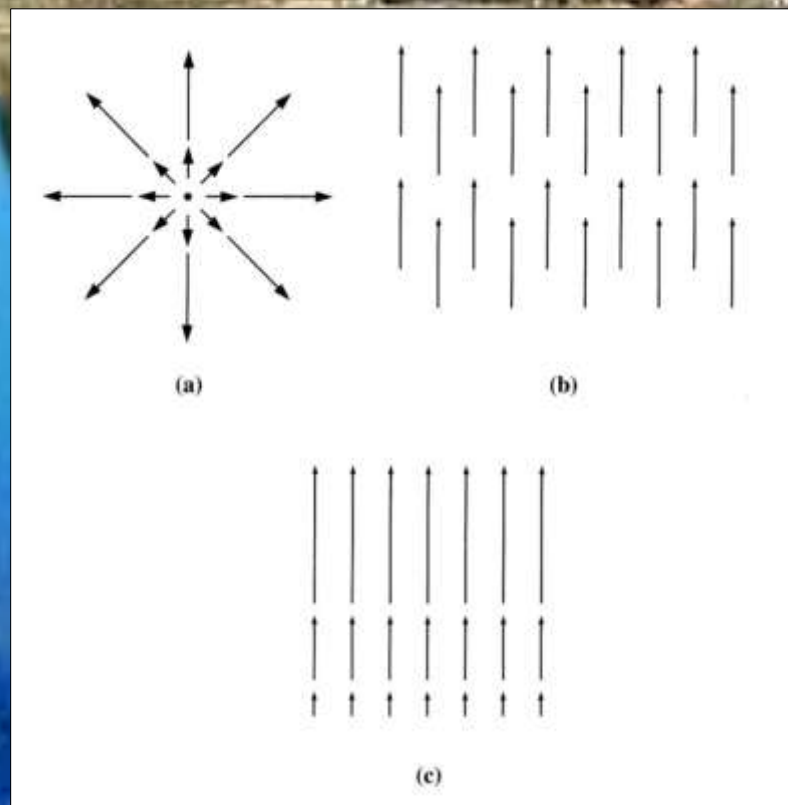
$$\nabla \cdot \mathbf{A}(\vec{r}) = \lim_{\Delta v \rightarrow 0} \frac{\oiint_S \mathbf{A}(\vec{r}) \cdot \overline{ds}}{\Delta v}$$

where the surface  $S$  is a **closed** surface that **completely** surrounds a **very small** volume  $\Delta v$  at point  $\vec{r}$ , and where  $\overline{ds}$  points **outward** from the closed surface.

If you know gradient everywhere, can you tell me what the scalar field is???



# Divergence



*Pine needles in a pond...*

# Vector fields have spatial variability

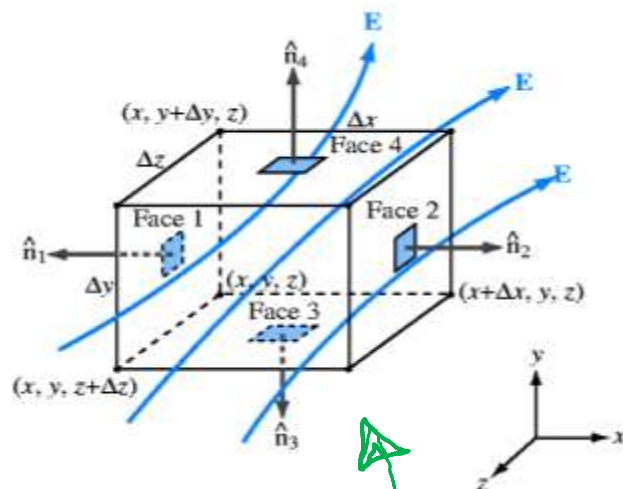
The mathematical definition of divergence is:

$$\nabla \cdot \mathbf{A}(\bar{r}) = \lim_{\Delta v \rightarrow 0} \frac{\oiint_S \mathbf{A}(\bar{r}) \cdot d\bar{s}}{\Delta v}$$

where the surface  $S$  is a **closed** surface that **completely** surrounds a **very small** volume  $\Delta v$  at point  $\bar{r}$ , and where  $d\bar{s}$  points **outward** from the closed surface.

$\vec{A}$  is a vector field

$\text{div } \vec{A} = \nabla \cdot \vec{A}$  is a scalar field!

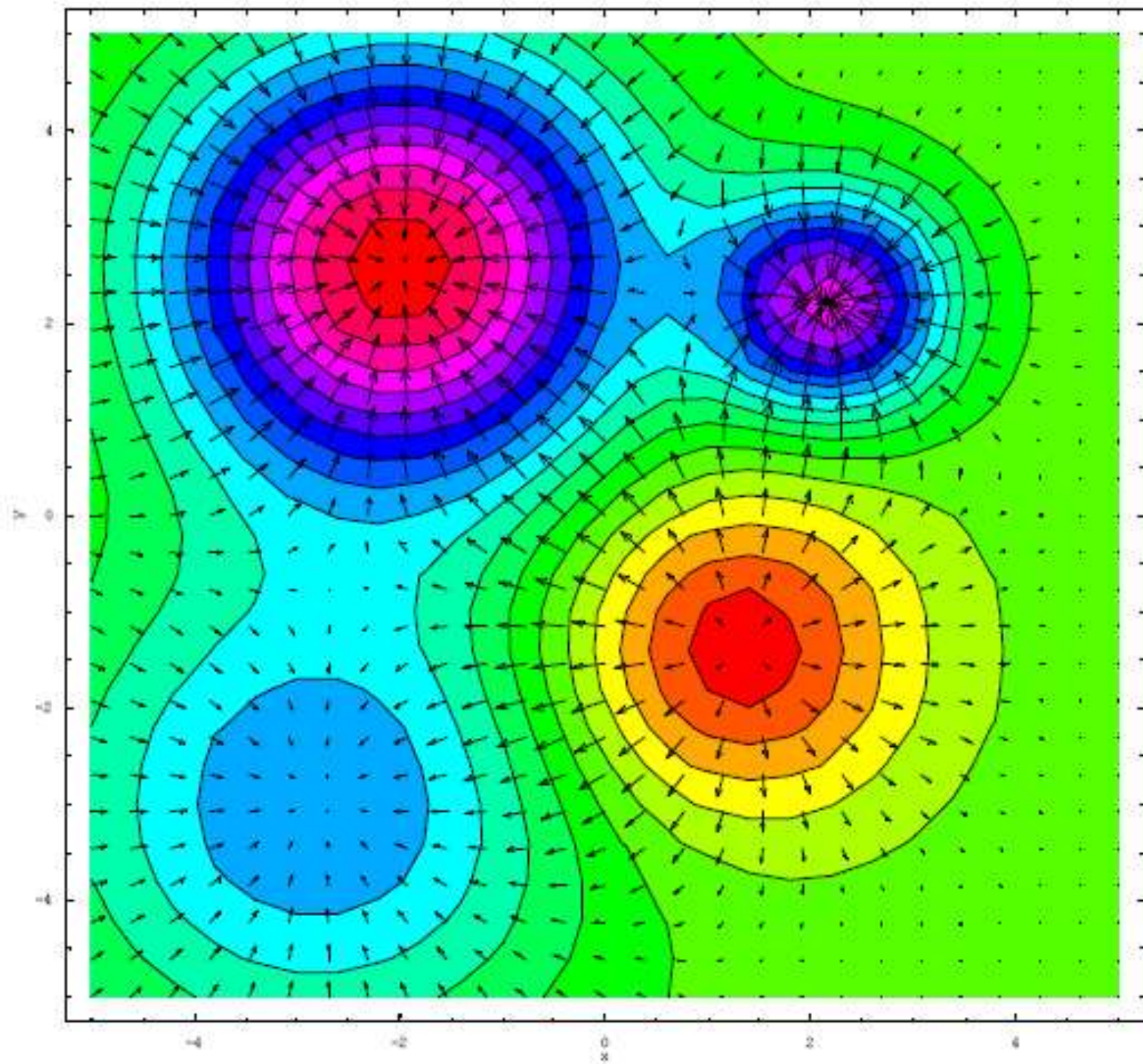


$$\nabla \cdot \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

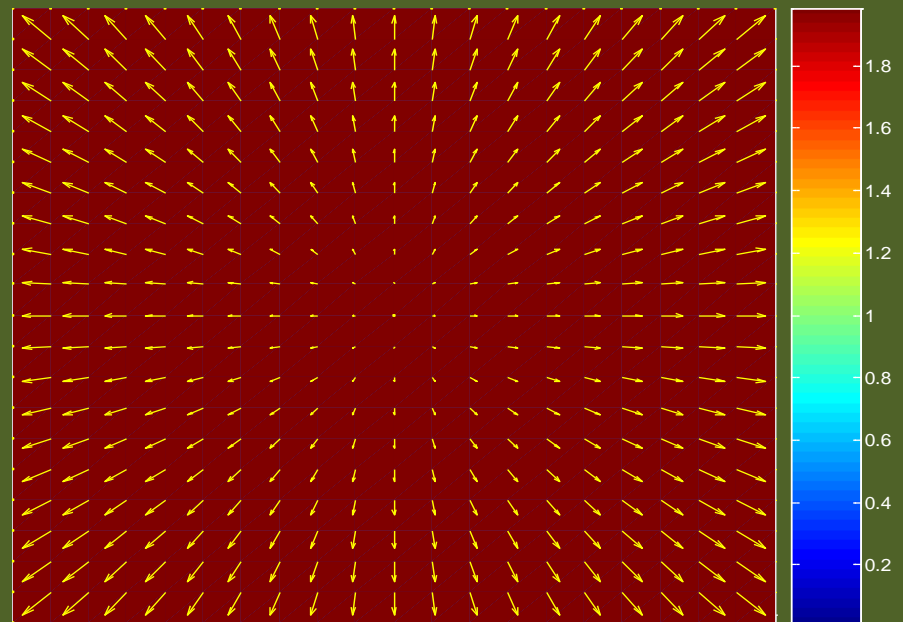
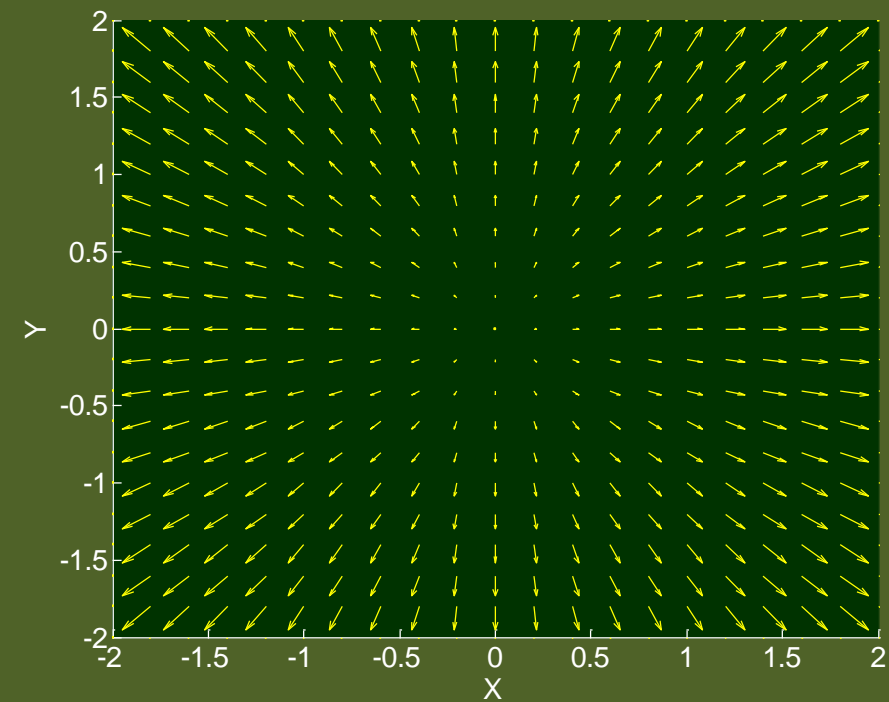
$$\nabla \cdot \mathbf{A} = \frac{1}{R^2} \frac{\partial}{\partial R} (R^2 A_R) + \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$





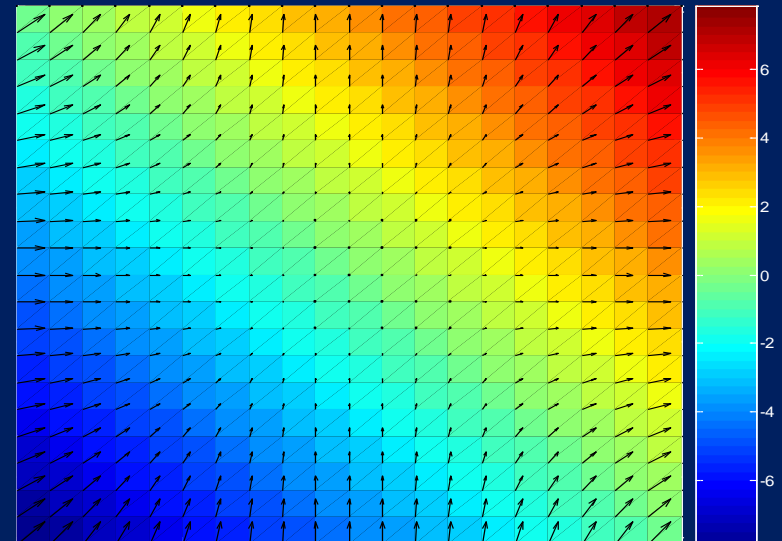
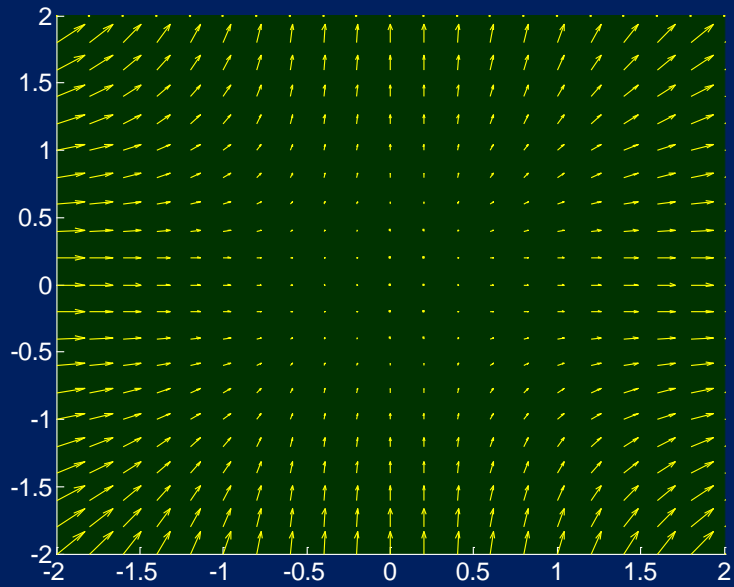
$$\vec{V} = x\hat{x} + y\hat{y}$$

$$\nabla \cdot \vec{V} = 2$$



$$\vec{V} = x^2 \hat{x} + y^2 \hat{y}$$

$$\nabla \cdot \vec{V} = 2x + 2y$$





# Divergence Theorem

(or Gauss', or Green's, etc.)

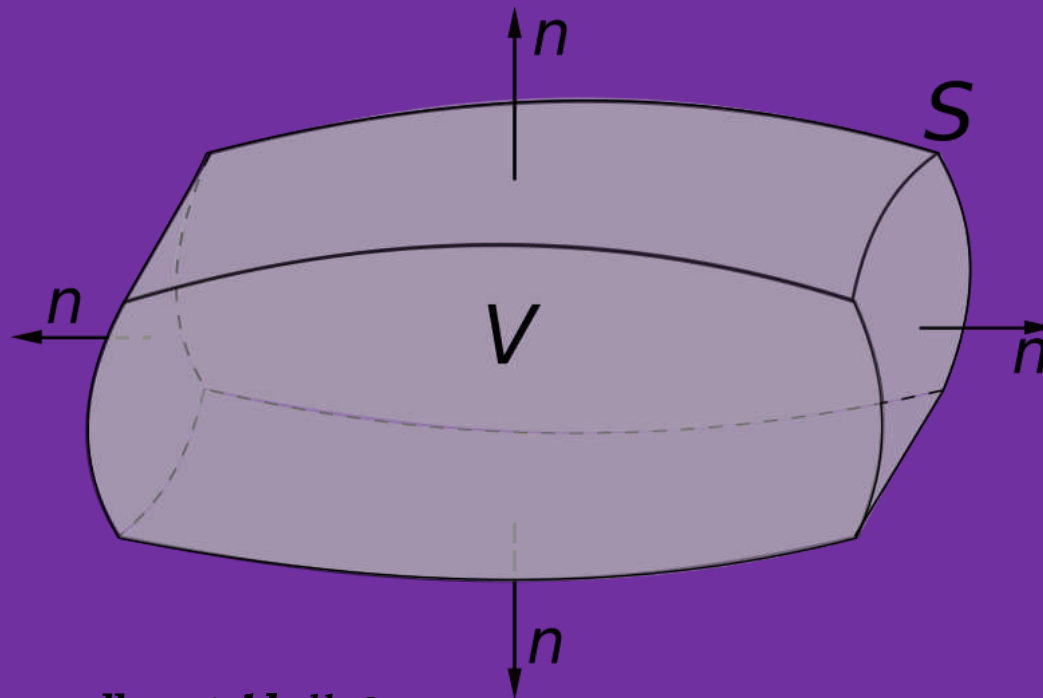
$$\int_V (\nabla \cdot \vec{V}) d\tau = \oint_S \vec{V} \cdot d\vec{a}$$

or  $dV$

or  $d\vec{s}$

Volume

Closed Surface containing Volume  $V$

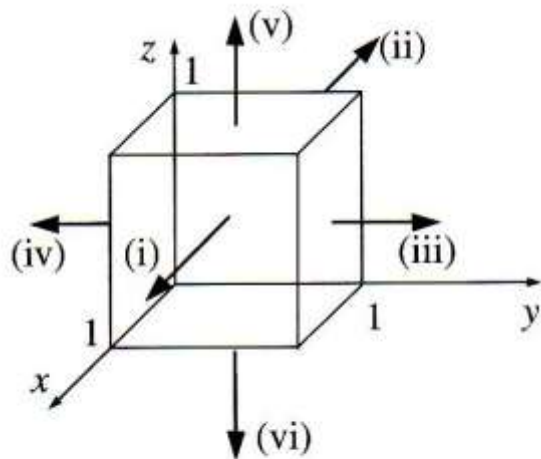


BTW... variables are, well, variable !! ☺

Check the divergence theorem using the function

$$\mathbf{v} = y^2 \hat{\mathbf{x}} + (2xy + z^2) \hat{\mathbf{y}} + (2yz) \hat{\mathbf{z}}$$

and the unit cube situated at the origin



**Solution:** In this case

$$\nabla \cdot \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla \cdot \mathbf{v} = 2(x + y),$$

and

$$\int_V 2(x + y) d\tau = 2 \int_0^1 \int_0^1 \int_0^1 (x + y) dx dy dz,$$
$$\int_0^1 (x + y) dx = \frac{1}{2} + y, \quad \int_0^1 (\frac{1}{2} + y) dy = 1, \quad \int_0^1 1 dz = 1.$$

Evidently,

$$\int_V \nabla \cdot \mathbf{v} d\tau = 2.$$

So much for the left side of the divergence theorem. To evaluate the surface integral we must consider separately the six sides of the cube:

- (i)  $\int \mathbf{v} \cdot d\mathbf{a} = \int_0^1 \int_0^1 y^2 dy dz = \frac{1}{3}.$
- (ii)  $\int \mathbf{v} \cdot d\mathbf{a} = - \int_0^1 \int_0^1 y^2 dy dz = -\frac{1}{3}.$
- (iii)  $\int \mathbf{v} \cdot d\mathbf{a} = \int_0^1 \int_0^1 (2x + z^2) dx dz = \frac{4}{3}.$
- (iv)  $\int \mathbf{v} \cdot d\mathbf{a} = - \int_0^1 \int_0^1 z^2 dx dz = -\frac{1}{3}.$
- (v)  $\int \mathbf{v} \cdot d\mathbf{a} = \int_0^1 \int_0^1 2y dx dy = 1.$
- (vi)  $\int \mathbf{v} \cdot d\mathbf{a} = - \int_0^1 \int_0^1 0 dx dy = 0.$

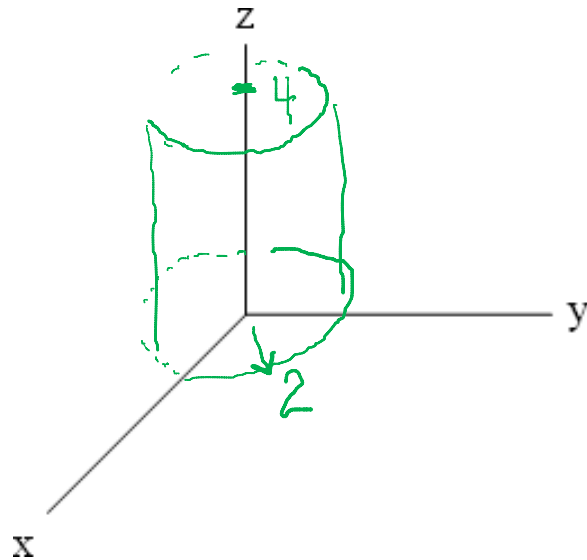
So the total flux is:

$$\oint_S \mathbf{v} \cdot d\mathbf{a} = \frac{1}{3} - \frac{1}{3} + \frac{4}{3} - \frac{1}{3} + 1 + 0 = 2,$$

as expected.

**Problem 3.40** For the vector field  $\mathbf{E} = \hat{\mathbf{r}}10e^{-r} - \hat{\mathbf{z}}3z$ , verify the divergence theorem for the cylindrical region enclosed by  $r = 2$ ,  $z = 0$ , and  $z = 4$ .

**Solution:**



$$ds_r = \hat{\mathbf{r}} r d\phi dz$$

$$ds_\phi = \hat{\phi} dr dz$$

$$ds_z = \hat{\mathbf{z}} r dr d\phi$$

$$r dr d\phi dz$$

$$\begin{aligned} \oint \mathbf{E} \cdot d\mathbf{s} &= \int_{r=0}^2 \int_{\phi=0}^{2\pi} ((\hat{\mathbf{r}}10e^{-r} - \hat{\mathbf{z}}3z) \cdot (-\hat{\mathbf{z}}r dr d\phi)) \Big|_{z=0} \\ &+ \int_{\phi=0}^{2\pi} \int_{z=0}^4 ((\hat{\mathbf{r}}10e^{-r} - \hat{\mathbf{z}}3z) \cdot (\hat{\mathbf{r}}r d\phi dz)) \Big|_{r=2} \\ &+ \int_{r=0}^2 \int_{\phi=0}^{2\pi} ((\hat{\mathbf{r}}10e^{-r} - \hat{\mathbf{z}}3z) \cdot (\hat{\mathbf{z}}r dr d\phi)) \Big|_{z=4} \\ &= 0 + \int_{\phi=0}^{2\pi} \int_{z=0}^4 10e^{-2} 2 d\phi dz + \int_{r=0}^2 \int_{\phi=0}^{2\pi} -12r dr d\phi \\ &= 160\pi e^{-2} - 48\pi \approx -82.77, \end{aligned}$$

$$\begin{aligned} \iiint \nabla \cdot \mathbf{E} d\mathcal{V} &= \int_{z=0}^4 \int_{r=0}^2 \int_{\phi=0}^{2\pi} \left( \frac{10e^{-r}(1-r)}{r} - 3 \right) r d\phi dr dz \\ &= 8\pi \int_{r=0}^2 (10e^{-r}(1-r) - 3r) dr \\ &= 8\pi \left( -10e^{-r} + 10e^{-r}(1+r) - \frac{3r^2}{2} \right) \Big|_{r=0}^2 \\ &= 160\pi e^{-2} - 48\pi \approx -82.77. \end{aligned}$$

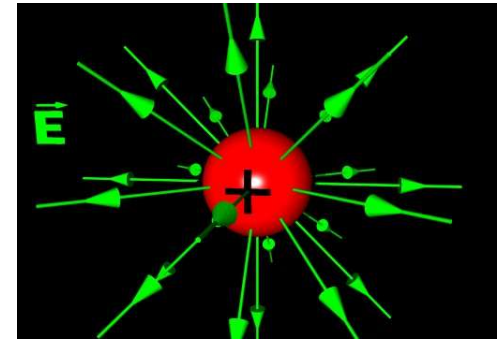
$$\nabla \cdot \mathbf{A} = \frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

# Vector fields have spatial variability

(EXAMPLE)

$$\vec{E} = \frac{1}{R^2} \hat{R}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{R^2} \frac{\partial}{\partial R} (R^2 A_R) + \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$



$$\Rightarrow \nabla \cdot \vec{E} = \frac{1}{R^2} \frac{\partial}{\partial R} \left( R^2 \frac{1}{R^2} \right) = 0$$

??

$$\int_V (\nabla \cdot \vec{V}) d\tau = \oint_S \vec{V} \cdot d\vec{a}$$

$$\begin{aligned} ds_R &= \hat{R} R^2 \sin \theta d\theta d\phi \\ ds_\theta &= \hat{\theta} R \sin \theta dR d\phi \\ ds_\phi &= \hat{\phi} R dR d\theta \end{aligned}$$

use imaginary sphere, Radius  $R$

$$\begin{aligned} \oint \vec{E} \cdot d\vec{s} &= \int \frac{1}{R^2} \hat{R} \cdot R^2 \sin \theta d\theta d\phi \hat{R} \\ &= \left( \int_0^\pi \sin \theta d\theta \right) \left( \int_0^{2\pi} d\phi \right) = 4\pi \end{aligned}$$

$$\int_V \nabla \cdot \vec{E} dV = 0?$$

What's up??  
 $0 \neq 4\pi$

not a function of  $R$

Gauss's law

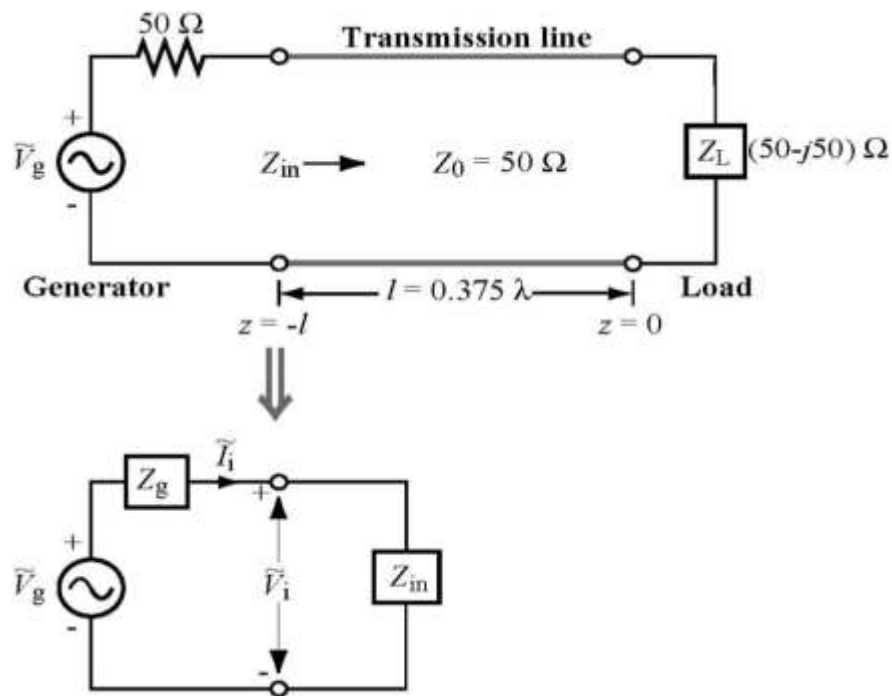
$$\nabla \cdot \mathbf{D} = \rho_v$$

$$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$$

# T-Line Example...

**Problem 2.30** A  $50\text{-}\Omega$  lossless line of length  $l = 0.375\lambda$  connects a 300-MHz generator with  $\tilde{V}_g = 300\text{ V}$  and  $Z_g = 50\text{ }\Omega$  to a load  $Z_L$ . Determine the time-domain current through the load for:

- (a)  $Z_L = (50 - j50)\text{ }\Omega$ ,
- (b)  $Z_L = 50\text{ }\Omega$ ,
- (c)  $Z_L = 0$  (short circuit).



**Solution:**

(a)  $Z_L = (50 - j50)\text{ }\Omega$   $\beta l = \frac{2\pi}{\lambda} \times 0.375\lambda = 2.36\text{ (rad)} = 135^\circ$ .

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{50 - j50 - 50}{50 - j50 + 50} = \frac{-j50}{100 - j50} = 0.45e^{-j63.43^\circ}$$

Application of Eq. (2.63) gives:

$$Z_{in} = Z_0 \left[ \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right] = 50 \left[ \frac{(50 - j50) + j50 \tan 135^\circ}{50 + j(50 - j50) \tan 135^\circ} \right] = (100 + j50)\text{ }\Omega$$

Using Eq. (2.66) gives

$$\begin{aligned} V_0^+ &= \left( \frac{\tilde{V}_g Z_{in}}{Z_g + Z_{in}} \right) \left( \frac{1}{e^{j\beta l} + \Gamma e^{-j\beta l}} \right) \\ &= \frac{300(100 + j50)}{50 + (100 + j50)} \left( \frac{1}{e^{j135^\circ} + 0.45e^{-j63.43^\circ} e^{-j135^\circ}} \right) \\ &= 150e^{-j135^\circ}\text{ (V)}, \\ \tilde{I}_L &= \frac{V_0^+}{Z_0} (1 - \Gamma) = \frac{150e^{-j135^\circ}}{50} (1 - 0.45e^{-j63.43^\circ}) = 2.68e^{-j108.44^\circ}\text{ (A)}, \\ i_L(t) &= \Re\{ \tilde{I}_L e^{j\omega t} \} \\ &= \Re\{ 2.68e^{-j108.44^\circ} e^{j6\pi \times 10^8 t} \} \\ &= 2.68 \cos(6\pi \times 10^8 t - 108.44^\circ)\text{ (A)}. \end{aligned}$$

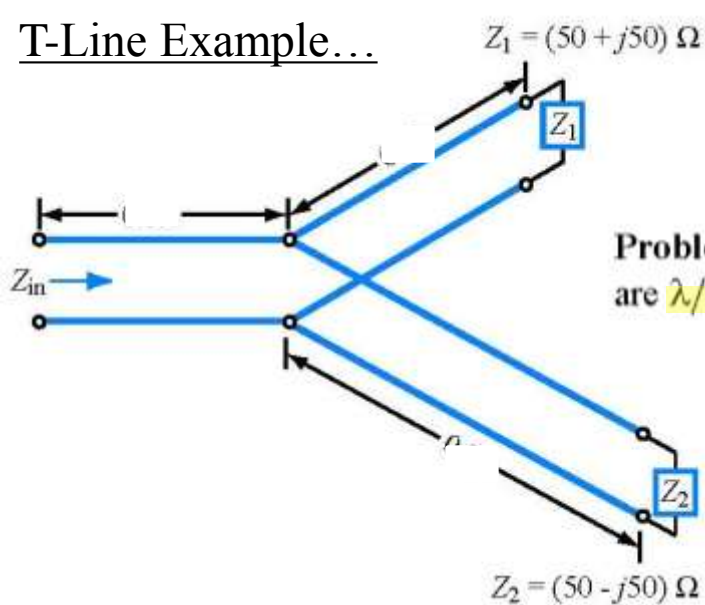
(b)

$$\begin{aligned} Z_L &= 50\text{ }\Omega, \\ \Gamma &= 0, \\ Z_{in} &= 50\text{ }\Omega, \\ V_0^+ &= \frac{300 \times 50}{50 + 50} \left( \frac{1}{e^{j135^\circ} + 0} \right) = 150e^{-j135^\circ}\text{ (V)}, \\ \tilde{I}_L &= \frac{V_0^+}{Z_0} = \frac{150}{50} e^{-j135^\circ} = 3e^{-j135^\circ}\text{ (A)}, \\ i_L(t) &= \Re\{ 3e^{-j135^\circ} e^{j6\pi \times 10^8 t} \} = 3 \cos(6\pi \times 10^8 t - 135^\circ)\text{ (A)}. \end{aligned}$$

(c)

$$\begin{aligned} Z_L &= 0, \\ \Gamma &= -1, \\ Z_{in} &= Z_0 \left( \frac{0 + jZ_0 \tan 135^\circ}{Z_0 + 0} \right) = jZ_0 \tan 135^\circ = -j50\text{ (}\Omega\text{)}, \\ V_0^+ &= \frac{300(-j50)}{50 - j50} \left( \frac{1}{e^{j135^\circ} - e^{-j135^\circ}} \right) = 150e^{-j135^\circ}\text{ (V)}, \\ \tilde{I}_L &= \frac{V_0^+}{Z_0} [1 - \Gamma] = \frac{150e^{-j135^\circ}}{50} [1 + 1] = 6e^{-j135^\circ}\text{ (A)}, \\ i_L(t) &= 6 \cos(6\pi \times 10^8 t - 135^\circ)\text{ (A)}. \end{aligned}$$

# T-Line Example...



**Problem 2.49** Repeat Problem 2.48 for the case where **all three** transmission lines are  **$\lambda/4$  in length**.

**Solution:** Since the transmission lines are in **parallel**, it is advantageous to express loads in terms of **admittances**. In the upper branch, which is a quarter wave line,

$$Y_{1 \text{ in}} = \frac{Y_0^2}{Y_1} = \frac{Z_1}{Z_0^2},$$

and similarly for the lower branch,

$$Y_{2 \text{ in}} = \frac{Y_0^2}{Y_2} = \frac{Z_2}{Z_0^2}.$$

Thus, the total load at the junction is

$$Y_{\text{JCT}} = Y_{1 \text{ in}} + Y_{2 \text{ in}} = \frac{Z_1 + Z_2}{Z_0^2}.$$

Therefore, since the common transmission line is also quarter-wave,

$$Z_{\text{in}} = Z_0^2 / Z_{\text{JCT}} = Z_0^2 Y_{\text{JCT}} = Z_1 + Z_2 = (50 + j50) \Omega + (50 - j50) \Omega = 100 \Omega.$$

“God created the integers...  
...all the rest is the work of man”

- **Leopold Kronecker**

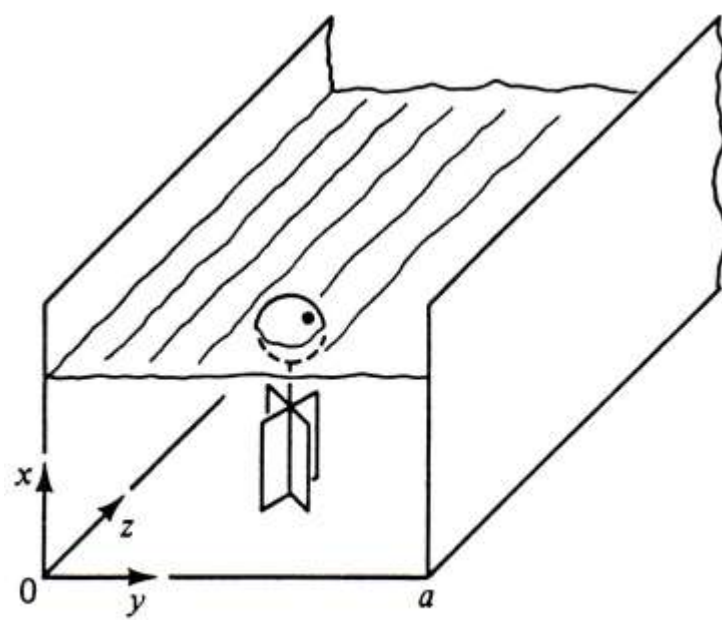
[http://en.wikipedia.org/wiki/Leopold\\_Kronecker](http://en.wikipedia.org/wiki/Leopold_Kronecker)

“A mathematician is a device for turning coffee into theorems.”

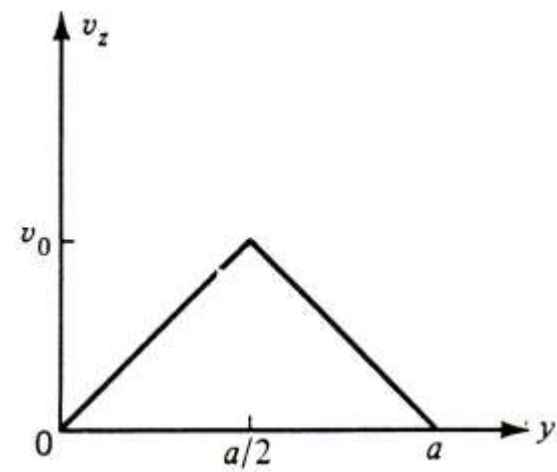
- **Paul Erdos**

[http://en.wikipedia.org/wiki/Paul\\_Erd%C5%91s](http://en.wikipedia.org/wiki/Paul_Erd%C5%91s)

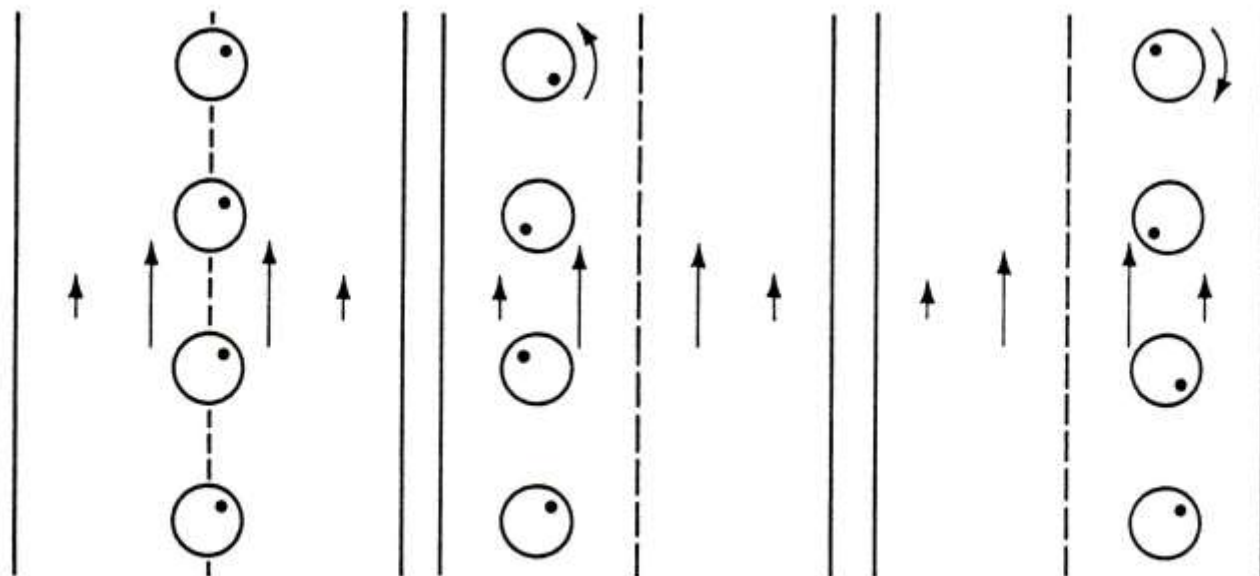




(a)



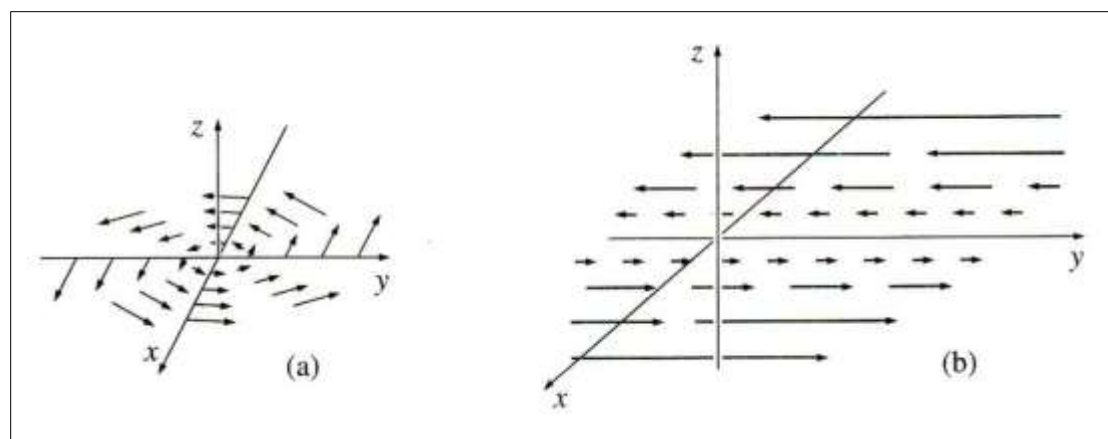
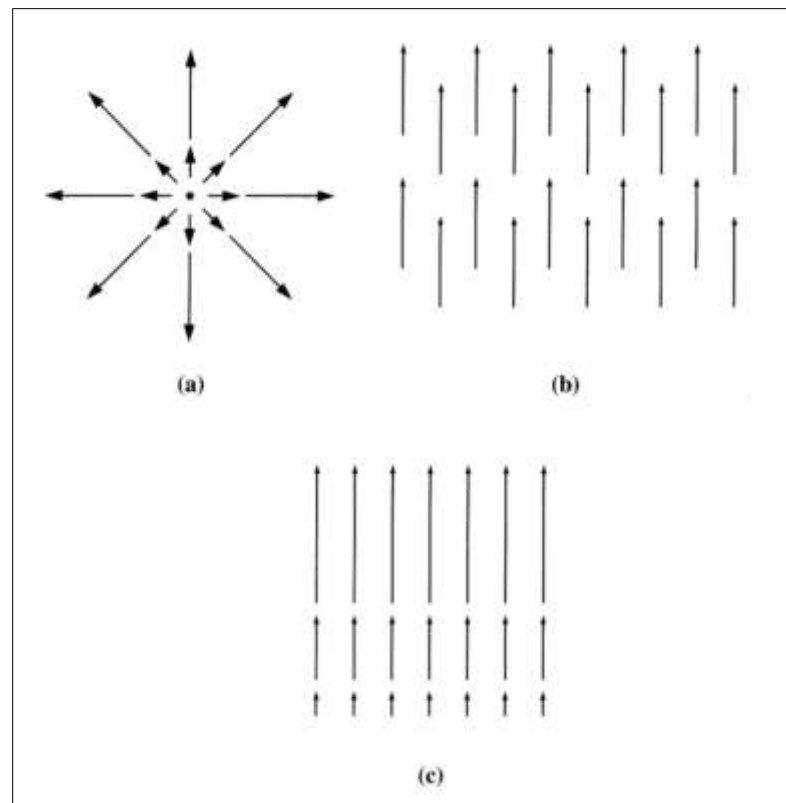
(b)



(c)

(d)

(e)

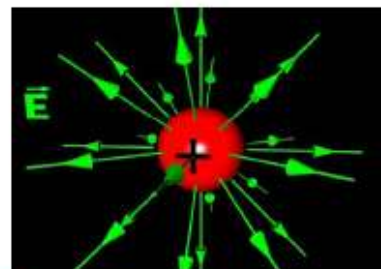


# Vector fields have spatial variability

(EXAMPLE)

$$\vec{E} = \frac{1}{R^2} \hat{R}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{R^2} \frac{\partial}{\partial R} (R^2 A_R) + \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$



$$\Rightarrow \nabla \cdot \vec{E} = \frac{1}{R^2} \frac{\partial}{\partial R} \left( R^2 \frac{1}{R^2} \right) = 0$$

??

$$\int_V (\nabla \cdot \vec{V}) d\tau = \oint_S \vec{V} \cdot d\vec{a}$$

$$\begin{aligned} ds_R &= R^2 \sin \theta d\theta d\phi \\ ds_\theta &= R \sin \theta dR d\phi \\ ds_\phi &= R dR d\theta \end{aligned}$$

use imaginary sphere, Radius R

$$\int_V \nabla \cdot \vec{E} dV = 0?$$

$$\begin{aligned} \oint \vec{E} \cdot d\vec{s} &= \int \frac{1}{R^2} \hat{R} \cdot R^2 \sin \theta d\theta d\phi \hat{R} \\ &= \left( \int_0^\pi \sin \theta d\theta \right) \left( \int_0^{2\pi} d\phi \right) = 4\pi \end{aligned}$$

not a function of R

What's up??  
 $0 \neq 4\pi$

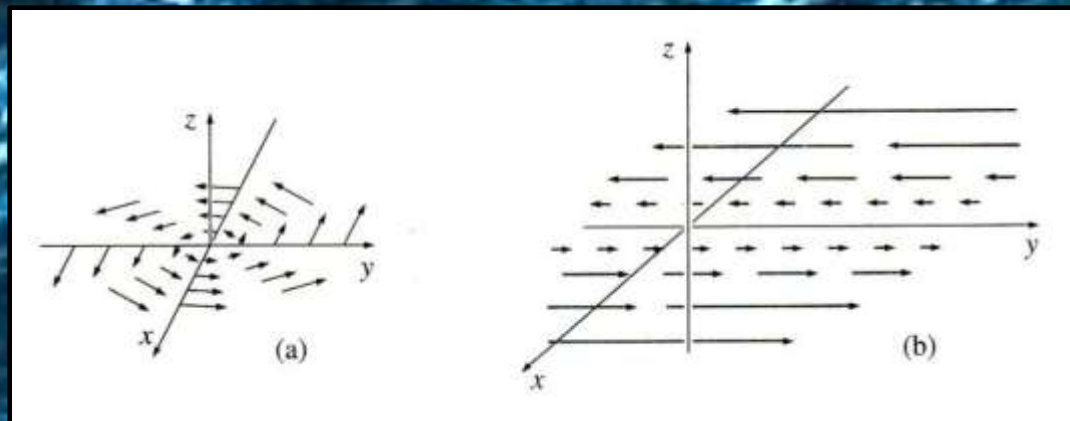
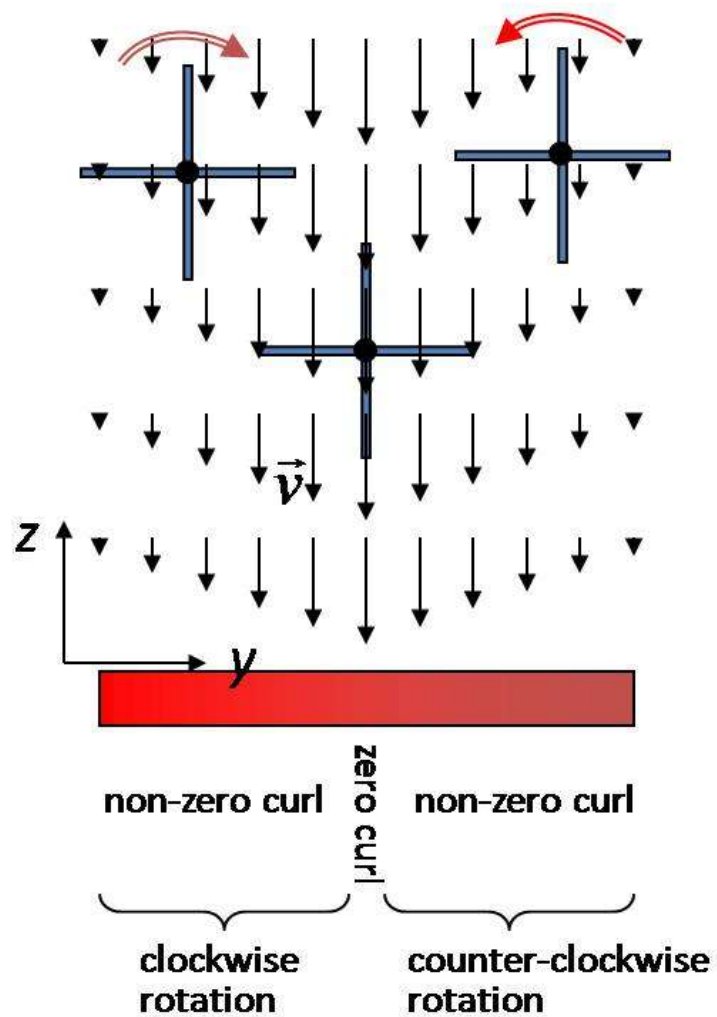
Gauss's law

$$\nabla \cdot \mathbf{D} = \rho_v$$

$$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q$$

# Curl

top view





# Vector fields have spatial variability

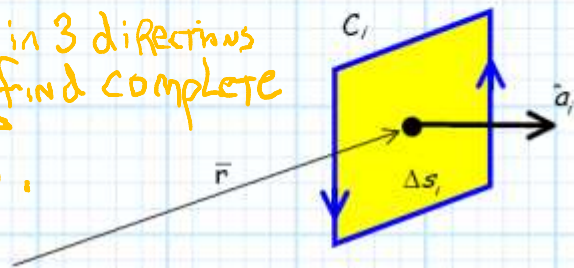
Say  $\nabla \times \mathbf{A}(\bar{r}) = \mathbf{B}(\bar{r})$ . The mathematical definition of Curl is given as:

$$B_i(\bar{r}) = \lim_{\Delta s \rightarrow 0} \frac{\oint_{C_i} \mathbf{A}(\bar{r}) \cdot d\vec{\ell}}{\Delta s_i}$$

This rather complex equation requires some **explanation** !

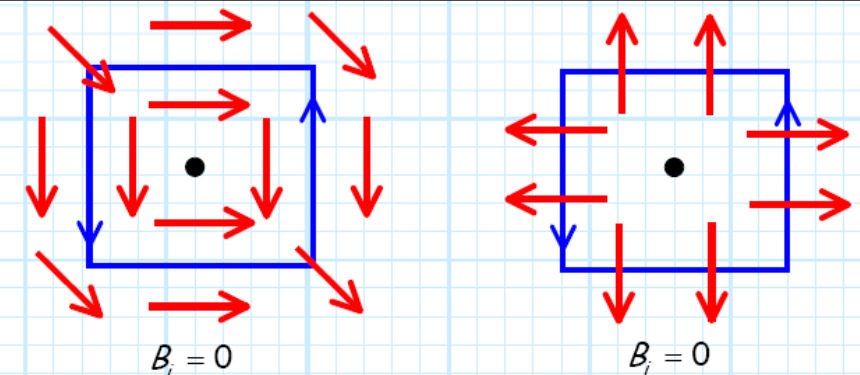
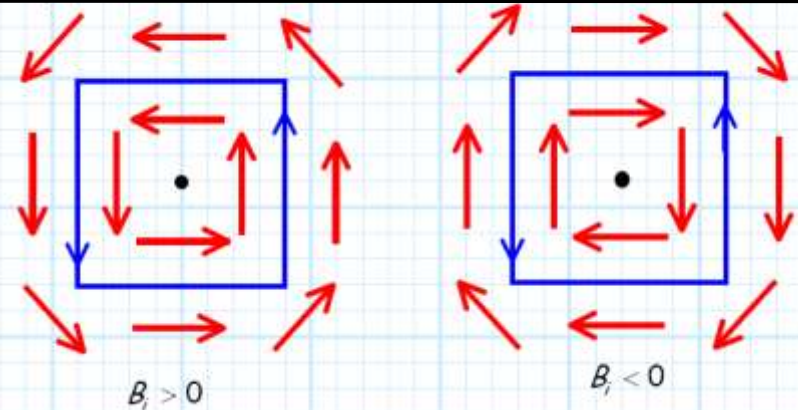
- \*  $B_i(\bar{r})$  is the scalar component of vector  $\mathbf{B}(\bar{r})$  in the direction defined by unit vector  $\hat{a}_i$  (e.g.,  $\hat{a}_x, \hat{a}_y, \hat{a}_z$ ).
- \* The small surface  $\Delta s_i$  is centered at point  $\bar{r}$ , and oriented such that it is normal to unit vector  $\hat{a}_i$ .
- \* The contour  $C_i$  is the closed contour that surrounds surface  $\Delta s_i$ .

Do in 3 directions  
to find complete  
 $\vec{B}$ .



If a component of vector field  $\mathbf{A}(\bar{r})$  is pointing in the direction  $d\vec{\ell}$  at every point on contour  $C_i$  (i.e., **tangential** to the contour). Then the line integral, and thus the curl, will be **positive**.

If, however, a component of vector field  $\mathbf{A}(\bar{r})$  points in the opposite direction ( $-d\vec{\ell}$ ) at every point on the contour, the curl at point  $\bar{r}$  will be **negative**.



Note: these are vanishingly *small* contours...

## Vector fields have spatial variability

$$\nabla \times \mathbf{A} = \begin{vmatrix} \hat{\mathbf{x}} & \hat{\mathbf{y}} & \hat{\mathbf{z}} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} = \hat{\mathbf{x}} \left( \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + \hat{\mathbf{y}} \left( \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + \hat{\mathbf{z}} \left( \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

### Example

$$\vec{A} = \hat{x}(1 + 2yz) - \hat{y}(x^2 + y^2) + \hat{z}(1 - 2yz) \quad \nabla \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 1 + 2yz & -(x^2 + y^2) & 1 - 2yz \end{vmatrix} = \hat{x}(-2z) + \hat{y}2y + \hat{z}(-2x - 2z)$$

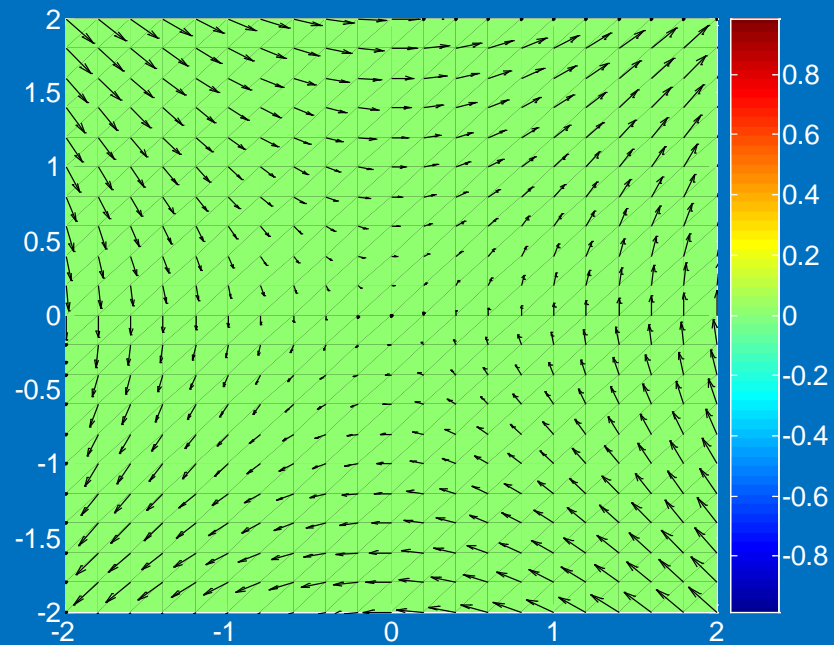
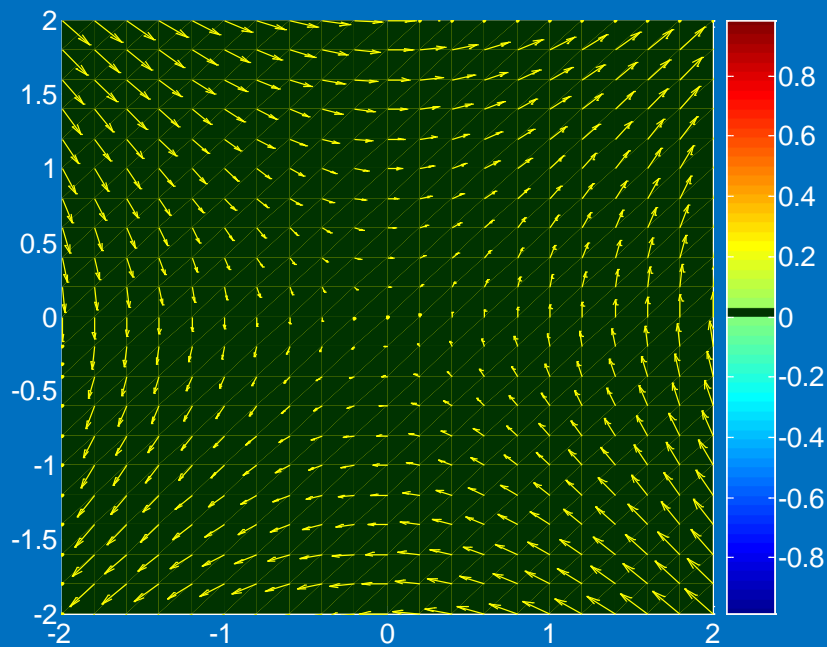
$$\nabla \times \mathbf{A} = \frac{1}{r} \begin{vmatrix} \hat{\mathbf{r}} & \hat{\boldsymbol{\phi}} r & \hat{\mathbf{z}} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_r & r A_\phi & A_z \end{vmatrix} = \hat{\mathbf{r}} \left( \frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \hat{\boldsymbol{\phi}} \left( \frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \hat{\mathbf{z}} \frac{1}{r} \left[ \frac{\partial}{\partial r} (r A_\phi) - \frac{\partial A_r}{\partial \phi} \right]$$

$$\begin{aligned} \nabla \times \mathbf{A} &= \frac{1}{R^2 \sin \theta} \begin{vmatrix} \hat{\mathbf{R}} & \hat{\boldsymbol{\theta}} R & \hat{\boldsymbol{\phi}} R \sin \theta \\ \frac{\partial}{\partial R} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_R & R A_\theta & (R \sin \theta) A_\phi \end{vmatrix} \\ &= \hat{\mathbf{R}} \frac{1}{R \sin \theta} \left[ \frac{\partial}{\partial \theta} (A_\phi \sin \theta) - \frac{\partial A_\theta}{\partial \phi} \right] + \hat{\boldsymbol{\theta}} \frac{1}{R} \left[ \frac{1}{\sin \theta} \frac{\partial A_R}{\partial \phi} - \frac{\partial}{\partial R} (R A_\phi) \right] + \hat{\boldsymbol{\phi}} \frac{1}{R} \left[ \frac{\partial}{\partial R} (R A_\theta) - \frac{\partial A_R}{\partial \theta} \right] \end{aligned}$$



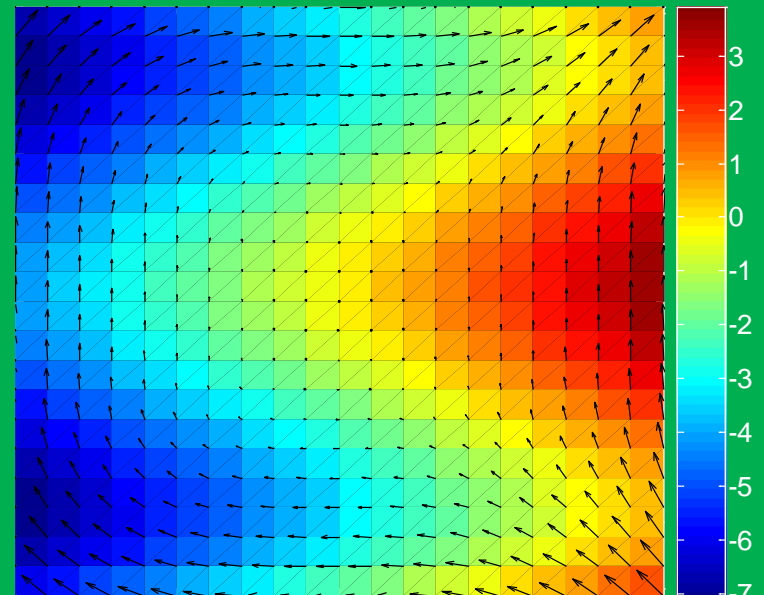
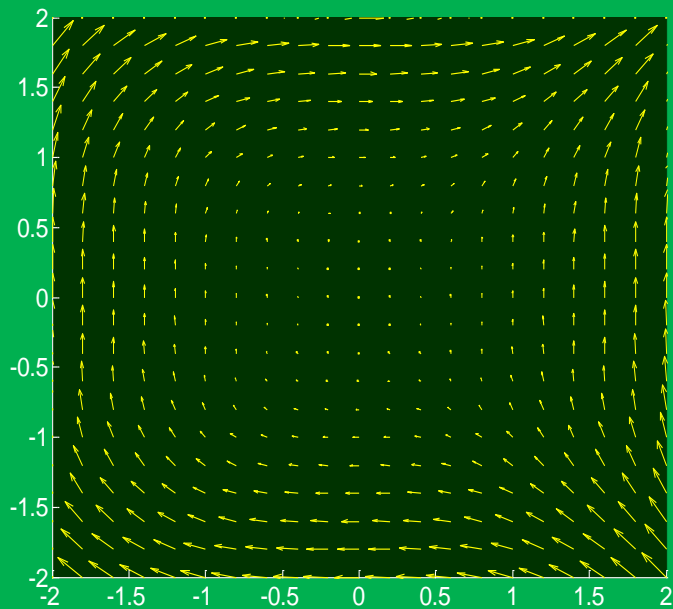
$$\vec{V} = x\hat{x} + y\hat{y} + 0\hat{z}$$

$$\nabla \times \vec{V} = 1 - 1 = 0$$



$$\vec{V} = y^2 \sin(y) \hat{\mathbf{x}} + x^2 \hat{\mathbf{y}} + 0 \hat{\mathbf{z}}$$

$$\nabla \times \vec{V} = (2x - 2y \sin(y) + y^2 \cos(y)) \hat{\mathbf{z}}$$



# Why DO we care about curl ???

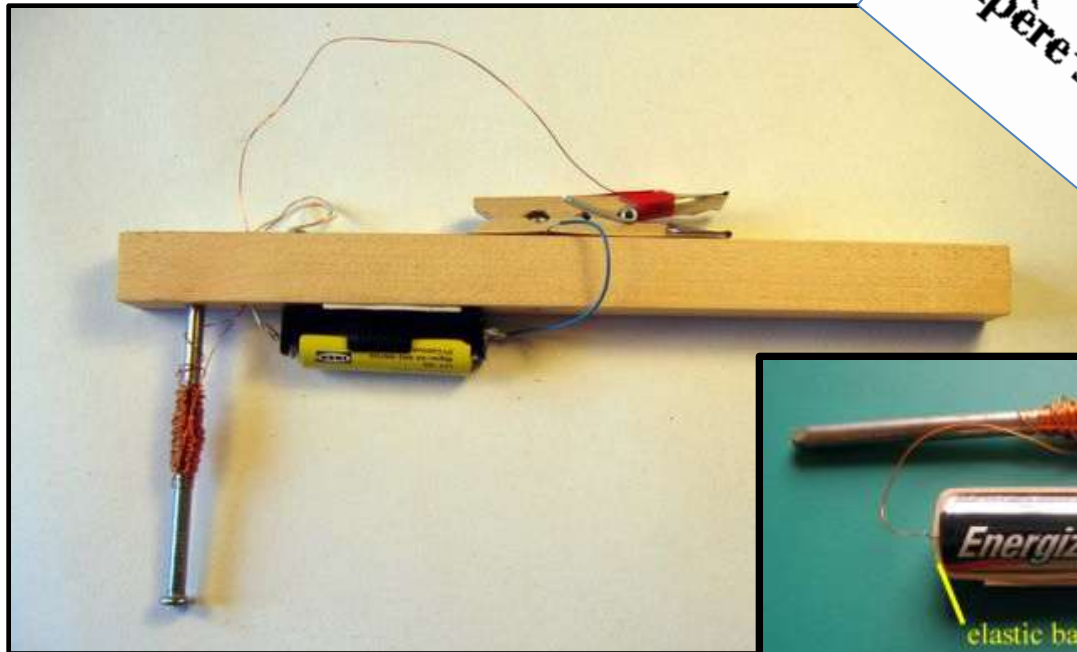
## Helmholtz Theorem

*If you know  $\nabla \cdot \mathbf{A}(\bar{\mathbf{r}})$  and you know  $\nabla \times \mathbf{A}(\bar{\mathbf{r}})$ , you have enough information to determine the vector field  $\mathbf{A}(\bar{\mathbf{r}})$ !*

Is this true????

Ampère's law

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$



# Stokes' Theorem

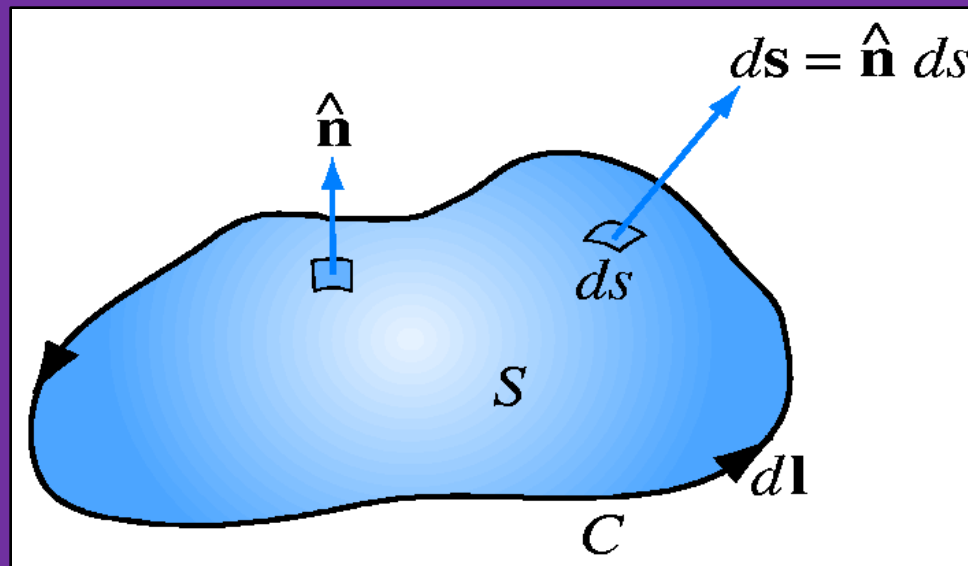
[http://en.wikipedia.org/wiki/George\\_Gabriel\\_Stokes](http://en.wikipedia.org/wiki/George_Gabriel_Stokes)

$$\int_S (\nabla \times \vec{V}) \cdot d\vec{a} = \oint_P \vec{V} \cdot d\vec{l}$$

$\nearrow S$   
Surface

$\nearrow$   
or  $d\vec{s}$   
(normal to surface)

$\longleftarrow P$  Path (or Contour)  
around edge of surface



[http://www.math.umn.edu/~rogness/multivar/multiple\\_surfaces.shtml](http://www.math.umn.edu/~rogness/multivar/multiple_surfaces.shtml)

BTW... variables are, well, variable !! ☺

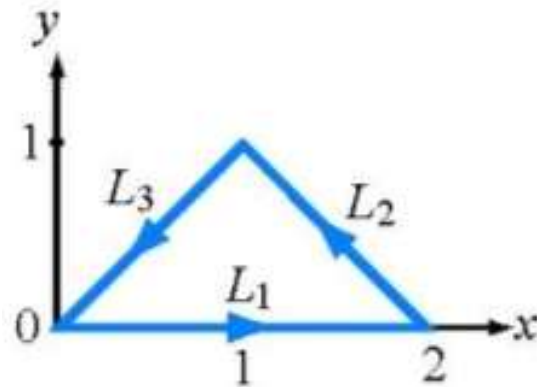
Q: what if  $S$  is a closed surface??

For the vector field  $\mathbf{E} = \hat{x}xy - \hat{y}(x^2 + 2y^2)$ , calculate

- (a)  $\oint_C \mathbf{E} \cdot d\mathbf{l}$  around the triangular contour shown  
 (b)  $\int_S (\nabla \times \mathbf{E}) \cdot d\mathbf{s}$  over the area of the triangle.

Differential length,  $d\mathbf{l} =$

$$\hat{x} dx + \hat{y} dy + \hat{z} dz$$



$$\nabla \times \mathbf{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} = \hat{x} \left( \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + \hat{y} \left( \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + \hat{z} \left( \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

Differential surface areas

$$\begin{aligned} ds_x &= \hat{x} dy dz \\ ds_y &= \hat{y} dx dz \\ ds_z &= \hat{z} dx dy \end{aligned}$$

**Solution:** In addition to the independent condition that  $z = 0$ , the three lines of the triangle are represented by the equations  $y = 0$ ,  $y = 2 - x$ , and  $y = x$ , respectively.

(a)

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = L_1 + L_2 + L_3,$$

$$\begin{aligned} L_1 &= \int (\hat{x}xy - \hat{y}(x^2 + 2y^2)) \cdot (\hat{x} dx + \hat{y} dy + \hat{z} dz) \\ &= \int_{x=0}^2 (xy)|_{y=0, z=0} dx - \int_{y=0}^0 (x^2 + 2y^2)|_{z=0} dy + \int_{z=0}^0 (0)|_{y=0} dz = 0, \end{aligned}$$

$$\begin{aligned} L_2 &= \int (\hat{x}xy - \hat{y}(x^2 + 2y^2)) \cdot (\hat{x} dx + \hat{y} dy + \hat{z} dz) \\ &= \int_{x=2}^1 (xy)|_{y=2-x, z=0} dx - \int_{y=0}^1 (x^2 + 2y^2)|_{x=2-y, z=0} dy + \int_{z=0}^0 (0)|_{y=2-x} dz \\ &= \left( x^2 - \frac{x^3}{3} \right) \Big|_{x=2}^1 - (4y - 2y^2 + y^3) \Big|_{y=0}^1 + 0 = -\frac{11}{3}, \end{aligned}$$

$$\begin{aligned} L_3 &= \int (\hat{x}xy - \hat{y}(x^2 + 2y^2)) \cdot (\hat{x} dx + \hat{y} dy + \hat{z} dz) \\ &= \int_{x=1}^0 (xy)|_{y=x, z=0} dx - \int_{y=1}^0 (x^2 + 2y^2)|_{x=y, z=0} dy + \int_{z=0}^0 (0)|_{y=x} dz \\ &= \left( \frac{x^3}{3} \right) \Big|_{x=1}^0 - (y^3) \Big|_{y=1}^0 + 0 = \frac{2}{3}. \end{aligned}$$

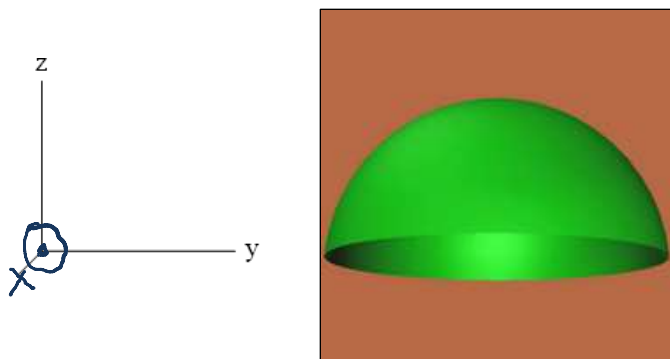
Therefore,

$$\oint_C \mathbf{E} \cdot d\mathbf{l} = 0 - \frac{11}{3} + \frac{2}{3} = -3.$$

(b) From Eq. (3.105),  $\nabla \times \mathbf{E} = -\hat{z}3x$ , so that

$$\begin{aligned} \iint_S \nabla \times \mathbf{E} \cdot d\mathbf{s} &= \int_{x=0}^1 \int_{y=0}^x ((-\hat{z}3x) \cdot (\hat{z} dy dx))|_{z=0} \\ &\quad + \int_{x=1}^2 \int_{y=0}^{2-x} ((-\hat{z}3x) \cdot (\hat{z} dy dx))|_{z=0} \\ &= - \int_{x=0}^1 \int_{y=0}^x 3x dy dx - \int_{x=1}^2 \int_{y=0}^{2-x} 3x dy dx \\ &= - \int_{x=0}^1 3x(x-0) dx - \int_{x=1}^2 3x((2-x)-0) dx \\ &= - (x^3) \Big|_0^1 - (3x^2 - x^3) \Big|_1^2 = -3. \end{aligned}$$

**Problem 3.47** Verify Stokes's Theorem for the vector field  $\mathbf{A} = \hat{\mathbf{R}} \cos \theta + \hat{\boldsymbol{\phi}} \sin \theta$  by evaluating it on the hemisphere of unit radius.



**Solution:**

$$\mathbf{A} = \hat{\mathbf{R}} \cos \theta + \hat{\boldsymbol{\phi}} \sin \theta = \hat{\mathbf{R}} A_R + \hat{\boldsymbol{\theta}} A_\theta + \hat{\boldsymbol{\phi}} A_\phi.$$

Hence,  $A_R = \cos \theta$ ,  $A_\theta = 0$ ,  $A_\phi = \sin \theta$ .

$$\begin{aligned} \nabla \times \mathbf{A} &= \hat{\mathbf{R}} \frac{1}{R \sin \theta} \left( \frac{\partial}{\partial \theta} (A_\phi \sin \theta) \right) - \hat{\boldsymbol{\theta}} \frac{1}{R} \frac{\partial}{\partial R} (R A_\phi) - \hat{\boldsymbol{\phi}} \frac{1}{R} \frac{\partial A_R}{\partial \theta} \\ &= \hat{\mathbf{R}} \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (\sin^2 \theta) - \hat{\boldsymbol{\theta}} \frac{1}{R} \frac{\partial}{\partial R} (R \sin \theta) - \hat{\boldsymbol{\phi}} \frac{1}{R} \frac{\partial}{\partial \theta} (\cos \theta) \\ &= \hat{\mathbf{R}} \frac{2 \cos \theta}{R} - \hat{\boldsymbol{\theta}} \frac{\sin \theta}{R} + \hat{\boldsymbol{\phi}} \frac{\sin \theta}{R}. \end{aligned}$$

For the hemispherical surface,  $ds = \hat{\mathbf{R}} R^2 \sin \theta d\theta d\phi$ .

**Differential surface areas**

$$\begin{aligned} ds_R &= \hat{\mathbf{R}} R^2 \sin \theta d\theta d\phi \\ ds_\theta &= \hat{\boldsymbol{\theta}} R \sin \theta dR d\phi \\ ds_\phi &= \hat{\boldsymbol{\phi}} R dR d\theta \end{aligned}$$

$$\begin{aligned} &\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi/2} (\nabla \times \mathbf{A}) \cdot d\mathbf{s} \\ &= \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi/2} \left( \frac{\hat{\mathbf{R}} 2 \cos \theta}{R} - \hat{\boldsymbol{\theta}} \frac{\sin \theta}{R} + \hat{\boldsymbol{\phi}} \frac{\sin \theta}{R} \right) \cdot \hat{\mathbf{R}} R^2 \sin \theta d\theta d\phi \Big|_{R=1} \\ &= 4\pi R \frac{\sin^2 \theta}{2} \Big|_0^{\pi/2} \Big|_{R=1} = 2\pi. \end{aligned}$$

The contour  $C$  is the circle in the  $x$ - $y$  plane bounding the hemispherical surface.

$$\oint_C \mathbf{A} \cdot d\mathbf{l} = \int_{\phi=0}^{2\pi} (\hat{\mathbf{R}} \cos \theta + \hat{\boldsymbol{\phi}} \sin \theta) \cdot \hat{\boldsymbol{\phi}} R d\phi \Big|_{\theta=\pi/2} = R \sin \theta \int_0^{2\pi} d\phi \Big|_{R=1} = 2\pi.$$

**Differential length,  $d\mathbf{l}$  =**

$$\hat{\mathbf{R}} dR + \hat{\boldsymbol{\theta}} R d\theta + \hat{\boldsymbol{\phi}} R \sin \theta d\phi$$



# Laplacian

The **scalar** Laplacian is simply **the divergence of the gradient** of a scalar field:

$$\nabla \cdot \nabla g(\vec{r})$$

The scalar Laplacian therefore both **operates** on a scalar field and **results** in a scalar field.

Often, the Laplacian is **denoted** as " $\nabla^2$ ", i.e.:

$$\nabla^2 g(\vec{r}) \doteq \nabla \cdot \nabla g(\vec{r})$$

From the expressions of divergence and gradient, we find that the scalar Laplacian is expressed in **Cartesian** coordinates as:

$$\nabla^2 g(\vec{r}) = \frac{\partial^2 g(\vec{r})}{\partial x^2} + \frac{\partial^2 g(\vec{r})}{\partial y^2} + \frac{\partial^2 g(\vec{r})}{\partial z^2}$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2}$$

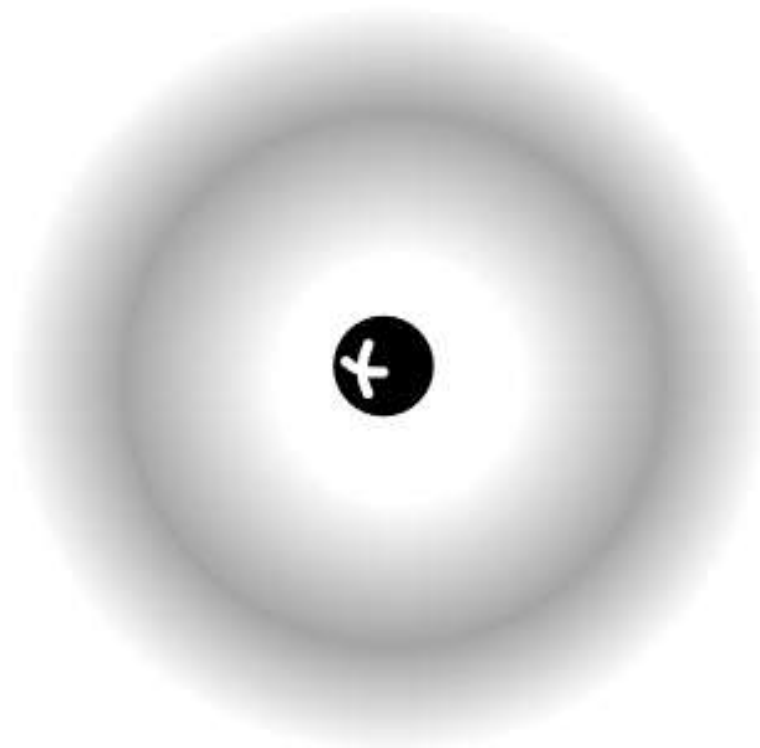
$$\nabla^2 V = \frac{1}{R^2} \frac{\partial}{\partial R} \left( R^2 \frac{\partial V}{\partial R} \right) + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{R^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

Example:

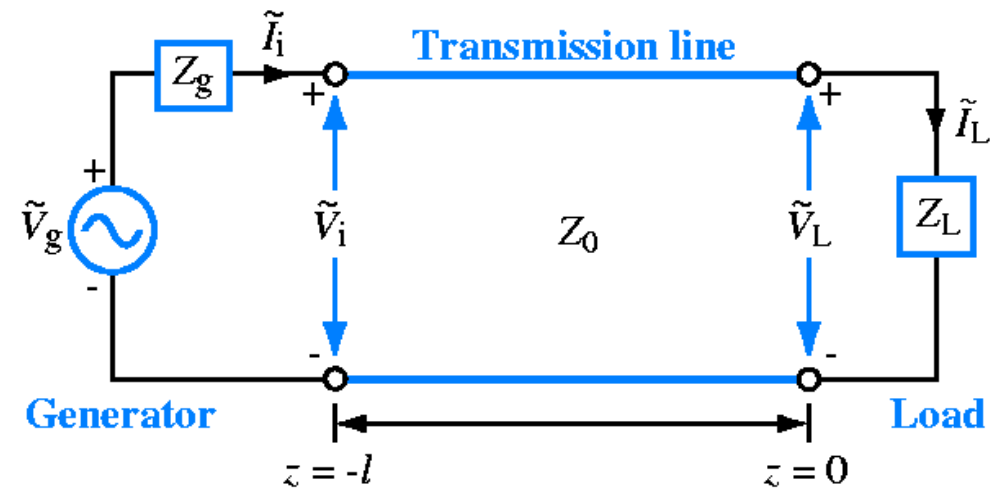
Find  $\nabla^2 \vec{A}$ , where  $\vec{A} = \hat{x}(1 + 2yz) - \hat{y}(x^2 + y^2) + \hat{z}(1 - 2yz)$

$$\nabla^2 \vec{A} =$$

$$\begin{aligned} &= \hat{x} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) (1 + 2yz) + \hat{y} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) (-x^2 - y^2) + \hat{z} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) (1 - 2yz) = \\ &= \hat{x}0 + \hat{y}(-2 - 2) + \hat{z}0 = -\hat{y}4 \end{aligned}$$



Why DO we care about the Laplacian ???



$$\begin{aligned} -\frac{d\tilde{V}(z)}{dz} &= (R' + j\omega L') \tilde{I}(z) \\ -\frac{d\tilde{I}(z)}{dz} &= (G' + j\omega C') \tilde{V}(z) \end{aligned}$$

$\nabla^2$  is the analog of this in 3-D for VECTOR fields (Like  $\vec{E}$ )

$$\frac{d^2 \tilde{V}(z)}{dz^2} = \gamma^2 \tilde{V}(z)$$

$$\tilde{V}(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z}$$

$$\tilde{V}(z) = V_0^+ e^{-\alpha z} e^{-j\beta z} \Rightarrow v(z,t) = V_0^+ e^{-\alpha z} \cos(\omega t - \beta z)$$

Traveling Wave 😊

## Triple Products

$$(1) \quad \mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) = \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) = \mathbf{C} \cdot (\mathbf{A} \times \mathbf{B})$$

$$(2) \quad \mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$$

## Product Rules

$$(3) \quad \nabla(fg) = f(\nabla g) + g(\nabla f)$$

$$(4) \quad \nabla(\mathbf{A} \cdot \mathbf{B}) = \mathbf{A} \times (\nabla \times \mathbf{B}) + \mathbf{B} \times (\nabla \times \mathbf{A}) + (\mathbf{A} \cdot \nabla)\mathbf{B} + (\mathbf{B} \cdot \nabla)\mathbf{A}$$

$$(5) \quad \nabla \cdot (f\mathbf{A}) = f(\nabla \cdot \mathbf{A}) + \mathbf{A} \cdot (\nabla f)$$

$$(6) \quad \nabla \cdot (\mathbf{A} \times \mathbf{B}) = \mathbf{B} \cdot (\nabla \times \mathbf{A}) - \mathbf{A} \cdot (\nabla \times \mathbf{B})$$

$$(7) \quad \nabla \times (f\mathbf{A}) = f(\nabla \times \mathbf{A}) - \mathbf{A} \times (\nabla f)$$

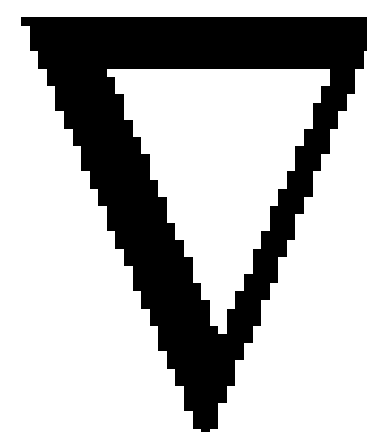
$$(8) \quad \nabla \times (\mathbf{A} \times \mathbf{B}) = (\mathbf{B} \cdot \nabla)\mathbf{A} - (\mathbf{A} \cdot \nabla)\mathbf{B} + \mathbf{A}(\nabla \cdot \mathbf{B}) - \mathbf{B}(\nabla \cdot \mathbf{A})$$

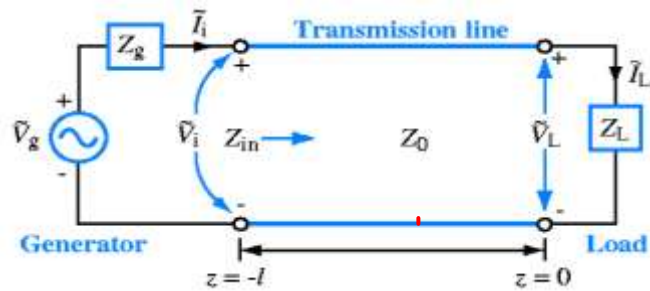
## Second Derivatives

$$(9) \quad \nabla \cdot (\nabla \times \mathbf{A}) = 0$$

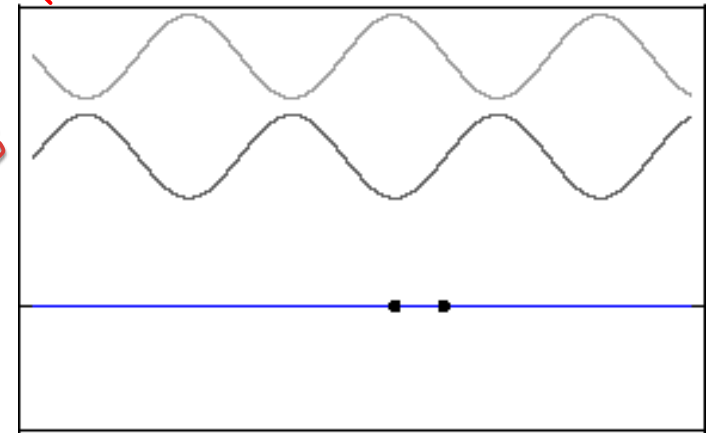
$$(10) \quad \nabla \times (\nabla f) = 0$$

$$(11) \quad \nabla \times (\nabla \times \mathbf{A}) = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}$$





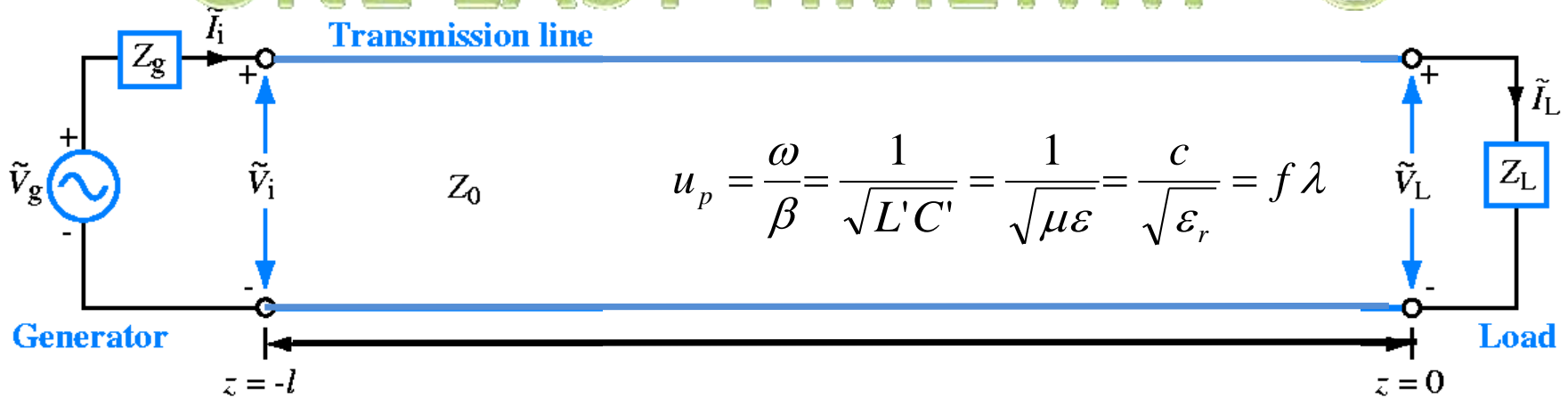
phase



$$\tilde{V}(z) = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z}$$

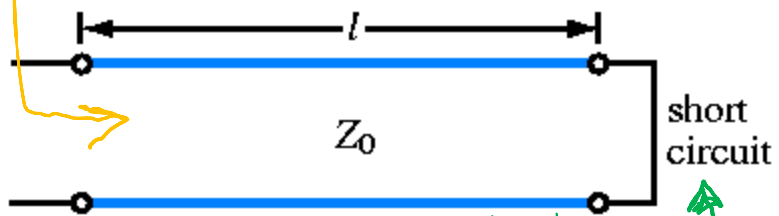
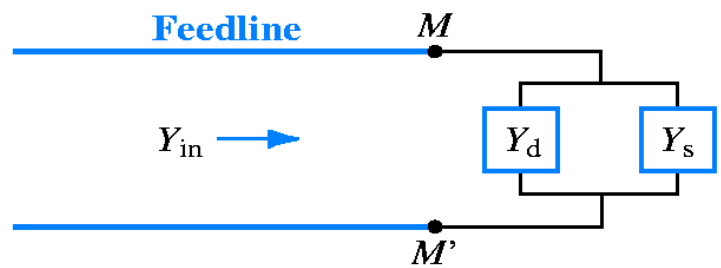
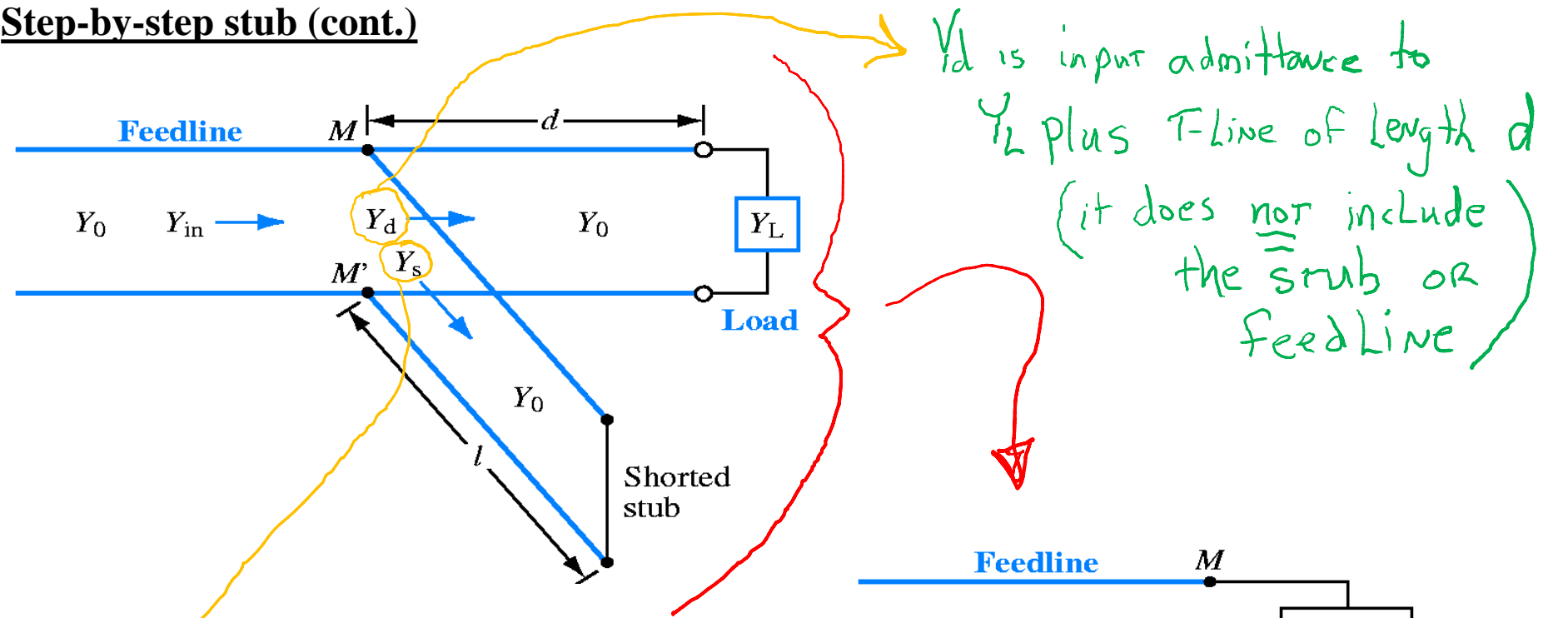
$$v(z, t) = |V_0^+| e^{-\alpha z} \cos(\omega t - \beta z + \phi^+) + |V_0^-| e^{\alpha z} \cos(\omega t + \beta z + \phi^-)$$

ONE LAST TIME!!!!!!



Sinusoidal Steady State vs. Transients

Step-by-step stub (cont.)



How's this all change if this is an open circuit

Another quick T-line thought:

at 60 GHz, wavelength is less than 5 mm...

...how does this impact circuit design at this frequency?



Finally, what is the angle between the vectors  $A$  and  $B$  at the point  $P(3,0,\pi)$ ?

find:

$$A \cdot B = \underline{\hspace{2cm}}$$

$$A \times B =$$

$$\nabla \cdot \mathbf{A} =$$

$$\nabla \times \mathbf{A} =$$

(10) Vectors in spherical coordinates can **not** be added directly.

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11) Voltage waves always travel at  $c$  down a lossless transmission line.

三

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If I know the gradient and the divergence at all points  
(as well as some boundary conditions) I can reproduce the field exactly.

T

F

$j^j$  has infinitely many values, all of which are real numbers.

T

F

The input impedance of a shorted stub can take on any value,  
depending on its length.

T

F

A given shorted stub behaves like an open circuit at 600 MHz. What is the closest frequency at which it behaves like a short (assuming constant phase speed)?

If  $\mathbf{A} = A_r \cos \theta \hat{\mathbf{R}}$ , evaluate  $\oint \nabla \times \mathbf{A} \cdot d\mathbf{s}$ , where the integration is over the surface of the unit sphere.

